

# Withdrawn

## Provided for Historical Reference Only

Carbon Monoxide in Workplace Atmospheres (Direct-Reading Monitor)



Method Number:	ID-209
Matrix:	Air
OSHA Permissible Exposure Limits (PEL)	
Final Rule*:	35 ppm Time Weighted Average (TWA) 200 ppm Ceiling (5-min sample) 1,500 ppm Instantaneous*
Transitional*:	50 ppm TWA
Monitoring Device:	Workplace areas are monitored using a direct-reading passive sampling instrument capable of recording data at given time intervals. Data can be retrieved after sampling.
Recommended Sampling Times:	
TWA Determination:	8 h
Ceiling Determination:	5 min
Analytical Procedure:	Direct-reading instrument - Datalogger. Data are transferred to a computer, exposures are calculated, and results are stored and/or sent to a printer for a hard copy.
Detection Limits (Instrument TWA read-out - also see Section 1.5.2)	
Qualitative:	1.2 ppm
Quantitative:	4.1 ppm
Precision and Accuracy:	TWA read-out                      Ceiling
CV <sub>2</sub> (Pooled):	0.040                                      0.032
Bias:	-0.016                                      -0.039
Overall Error:	±9.6%                                        ±10.5%
Validation Ranges:	16.1 to 70.2 ppm                      197.8 ppm
Special Requirements:	IBM-compatible computer
Method Classification:	Validated method (Direct Reading Instrument)
Chemist:	Robert G. Adler
Date:	March, 1993

\*This method was evaluated using the Final Rule Limits stated above; the Transitional Limit of 50 ppm is within tested ranges and the method should perform well when assessing compliance at this concentration. Compliance with the 1,500 ppm Instantaneous Exposure Limit [same as the Immediately Dangerous to Life and Health (IDLH)] cannot be assessed using the specific equipment described in this method. Please consult The OSHA Chemical Information File and Section 2 of this method regarding instantaneous carbon monoxide exposure determinations.

---

Commercial manufacturers and products mentioned in this method are for descriptive use only and do not constitute endorsements by USDOL-OSHA. Although the following Instrument Description, Backup Data, and Auxiliary Sampling (Appendix B) Sections of this report describe use of a specific carbon monoxide monitor, similar monitors can be substituted provided they meet validation requirements.

---

WITHDRAWN

Branch of Inorganic Methods Development  
OSHA Salt Lake Technical Center  
Salt Lake City, Utah

## 1. Introduction

### 1.1. History - Monitoring for Carbon Monoxide

The recent change in the OSHA Time Weighted Average (TWA) Permissible Exposure Limit (PEL) for CO from 50 to 35 ppm (5.1), the inclusion of a Ceiling PEL of 200 ppm (5-min sampling period) (5.2), and the addition of a maximum Instantaneous limit of 1,500 ppm (5.3) stimulated a review of the methods used for the analysis of CO in workplace atmospheres. This review included both direct-reading monitoring procedures and classical collection procedures.

The previous OSHA sampling and analytical method for CO required the use of direct-reading procedures for monitoring (5.4). One direct-reading procedure involved the use of CO short-term detector tubes (5.5). An evaluation at the OSHA Salt Lake Technical Center (OSHA-SLTC) was conducted for several brands of these tubes (5.6). Short-term detector tubes offer only spot checks of the environment, and sampling procedures capable of determining long-term CO concentrations are preferred. A long-term detector tube for CO was evaluated by OSHA and was determined to have significant lot-to-lot variability, and results were affected by sampling temperature (5.7). For TWA compliance measurements, a long-term direct-reading method was performed by OSHA compliance officers using an electrochemical detector (Ecolyzer, Energetics Science, Inc., Elmsford, NY). However, this instrument required constant calibration, readings were subject to drift, and TWA determinations were difficult to calculate. Due to the size of the instrument, only area samples were normally taken. Personal monitoring could be conducted by taking air samples in gas sampling bags and then attaching them to the Ecolyzer at the end of the sampling period. Air samples collected in gas bags or canisters have also been analyzed for CO using infrared absorption spectrophotometry (5.8), electrochemical means (5.9), gas chromatography (GC) with a flame ionization detector (FID) (5.10), or GC with a helium glow discharge ionization detector (DID) (5.11). A recently developed OSHA Method ID-210 (5.12) involves the use of gas bags followed by analysis by GC-DID. This is a reliable and sensitive method; however, it has the disadvantage of requiring sample shipment for laboratory analysis, and storage stability of the collected samples has to be addressed.

Recent developments in direct-reading instrumentation provide increased ease in personal monitoring of workplace atmospheres. These instruments are advertised as accurate and precise, and capable of storing data points for specified sampling periods (each period may be as small as 1 min). One such monitor is the Draeger Model 190 CO Datalogger (National Draeger, Inc., Pittsburgh, PA), which was the instrument evaluated for the current method. Other instruments may be substituted for monitoring CO provided they meet validation requirements.

### 1.2. Principle

Samples for monitoring exposures in regards to the TWA and 5-min Ceiling for CO are taken using a portable direct-reading instrument. A datalogger system can be used to reduce data to a TWA or 5-min Ceiling value. Other labor intensive methods such as hand-calculated averaging of readings, strip-chart-recordings, etc. can also be employed to reduce data if necessary.

### 1.3. Instrument Description and Special Features or Considerations

---

(Note: The Draeger Model 190 Datalogger is discussed below. Other commercially available monitors for CO may have similar characteristics.)

---

1.3.1. The Draeger Model 190 CO Datalogger consists of a patented 3-electrode diffusional electrochemical sensor with a removable filter cap, a liquid crystal display (LCD) for

providing direct-reading information, and a memory for storing the data. Logging of data may be started and ended by use of function keys (red and blue) provided. Sampled data are stored in 1-min intervals for a specified sampling time. The data can later be transferred to a computer or printer (5.13).

- 1.3.2. A CO-specific filter designed to reduce or eliminate any air contaminants which might interfere with the CO determination is available. This removable filter cap also serves as a dust filter. A plain dust filter can be attached to the sensor if the monitor is used where interfering contaminants are not present.
- 1.3.3. The operating temperature range is 0 to 40 °C. The optimum range in which minimal temperature effect occurs is 10 to 30 °C.
- 1.3.4. Recording of data:
  - 1.3.4.1. When the sensor is in operation, measured values are sent to the microprocessor twice each second. The values (120 sequential readings) are then computed into a 1-min average and this value is stored in memory. When data are transferred to a printer, the 1-min averages can be listed and/or graphically plotted. The sensor has a response time of approximately 1 min for large changes in concentration.
  - 1.3.4.2. The 1-min averages are truncated to integer ppm CO values (i.e., for 6.9 ppm CO the Datalogger would give a value of 6 ppm). The TWA value reported by the instrument is the average of all truncated 1-min averages, and is also truncated to an integer ppm value. The truncated values will always be  $\leq$  the hand-calculated values.

---

Note: Hand-calculated averages were also obtained during this study; in these cases, all truncated 1-min averages were manually averaged and rounded to the nearest 0.1 ppm value.

---
  - 1.3.4.3. The instrument also notes the highest 1-min average over the sampling period, and reports this value as the peak concentration. The specific time that this peak occurs is indicated either graphically or in a sampling summary. Where duplicate highest 1-min averages occur, only the first occurrence is listed. Monitoring for the OSHA Ceiling PEL of 200 ppm CO requires the user to perform a hand-calculated average of 1-min readings over a 5-min sampling period. The peak concentration function of the Datalogger cannot be used in this instance because it reports out only the highest 1-min reading.
- 1.3.5. The instrument is not capable of measuring the Instantaneous Exposure Limit of 1,500 ppm due to the instrument range limitation of 0 to 999 ppm CO.
- 1.3.6. Calibration for routine monitoring should be performed near the manufacturer-recommended flow rate of 0.20 L/min. Higher flow rates over the monitor sensor during calibration result in higher monitor readings, possibly because of a slight pressure increase at the face of the sensor under these conditions. Under normal workplace monitoring conditions, the recommended calibration procedure should give satisfactory results.

#### 1.4. Advantages and Disadvantages

#### 1.4.1. Advantages

- 1.4.1.1. According to the manufacturer, the instrument is specific for CO when the Datalogger is equipped with a CO-specific filter (P/N 4510184). Interferences besides those mentioned by the manufacturer were discovered during the evaluation. See Section 1.6 for further details.
- 1.4.1.2. The monitor is equipped with an audible alarm for immediate warning of dangerous CO levels.
- 1.4.1.3. The monitor can be used to measure compliance with Indoor Air Quality (IAQ) Standards for CO [9 ppm (8 h), 35 ppm (1 h)] (5.14).
- 1.4.1.4. The monitor is easy to set up and use and has a rapid response time (~1 min).
- 1.4.1.5. Data can be retrieved at the convenience of the industrial hygienist.
- 1.4.1.6. The monitor normally will not interfere with the worker's activities and is intrinsically safe if not altered.
- 1.4.1.7. Changes in humidity do not affect sample data collection.
- 1.4.1.8. The monitors permit measurement of the fluctuations in the CO concentration throughout the sampling period. Classical sample collection techniques will give only a TWA concentration unless multiple samples are taken.
- 1.4.1.9. The TWA concentration for the sampling period is calculated by the monitor. Peak concentrations are also indicated; however, a 5-min hand-calculated average is necessary when comparing output to the OSHA Ceiling PEL for CO.
- 1.4.1.10. Sample storage stability problems are not encountered.

#### 1.4.2. Disadvantages regarding equipment required or used for this procedure are:

- 1.4.2.1. Without a CO-specific filter, significant interferences can be encountered from ethylene, acetylene, hydrogen, hydrogen sulfide, nitrogen dioxide, nitric oxide, and sulfur dioxide. See Section 1.6 for other interferences.
- 1.4.2.2. For the initial purchase, the monitors are relatively expensive.
- 1.4.2.3. Additional equipment is needed for calibration. For accurate calibration, the calibration gas flow must be maintained at the manufacturer's recommended rate (0.20 L/min). For OSHA compliance, monitors are calibrated each time they are used.
- 1.4.2.4. Recovery of the data requires transferring to a computer or printer; sample results can be easily lost if the transfer is performed incorrectly. Data can also be lost if battery voltage drops significantly before the data can be transferred. A 9-volt battery is used to operate the instrument.
- 1.4.2.5. Samples taken in areas of high air velocities directed toward the sensor may result in a positive bias to the CO concentrations read.
- 1.4.2.6. Because the instrument automatically performs integer math for calculations, truncation error is possible for TWA values reported by the instrument, especially at single digit levels (i.e., <10 ppm). Optimal performance can be achieved if a hand-calculated average is obtained for all of the 1-min values

reported for a sampling period; however, this is a very tedious process and is not recommended for routine applications. The comparability of the precision and accuracy results in this study for the two calculation procedures indicates that, for CO levels near the TWA PEL, the extra calculation work is not necessary.

1.5. Method Performance (See Section 4 for more detailed information)

---

Note: During the evaluation, six instruments were used for each experiment. Imprecision was likely greater than if only one instrument were used and the experiment repeated six times; however, the statistical values obtained will be more representative of OSHA field office use. Many OSHA field offices are supplied with five or more monitors and an industrial hygienist may randomly take one or more instruments into the field for monitoring. As previously discussed in Section 1.3.4, both truncated and hand-calculated averages were used to determine instrument performance. The hand-calculated average only appears beneficial if detection limit is a significant factor as shown below.

---

1.5.1. Range

The upper analytical range used during the TWA PEL studies was about 70 ppm. The Ceiling study was conducted at about 200 ppm. The overall range according to the manufacturer is 0-999 ppm CO (5.13).

1.5.2. Precision, Accuracy, Detection Limits

Values determined during the validation are listed below. For further information see Section 4.

Statistical Data:

	Truncated	Hand-Calculated
Range*		
% Mean Recovery	96.1 - 112.4	96.6 - 114.0
CV (Individual experiments)	0.024 - 0.058	0.021 - 0.056
Bias	-0.016 - 0.062	-0.007 - 0.075
CV <sub>2</sub> (Pooled)	0.040 - 0.048	0.032 - 0.045

\* Includes different RHs and concns - 30 to 80% RH, 16.1 to 70.2 ppm

Detection Limits

Qualitative:	1.2 ppm	0.5 ppm
Quantitative:	4.1 ppm	1.8 ppm

Precision and Accuracy\*\*

CV <sub>2</sub> (Pooled):	0.040	0.041
Bias:	-0.016	-0.007
Overall Errors:	±9.6%	±8.8%

\*\* Only data for 0.5 to 2 times PEL, 50% RH is listed

1.6. Interference

---

Note: The following paragraphs list specific interferences associated with the Draeger Datalogger. If other types of instruments are used, always consult with the manufacturer or manufacturer-provided instructional manuals concerning potential interferences before general use. Additional information regarding interferences concerning the Draeger Datalogger can be found in reference 5.13.

The following interferences occur with the CO-specific filter attached to the monitor. Acetylene and hydrogen have small positive interferences (97 ppm acetylene will indicate 10 ppm CO, 1,000 ppm hydrogen will indicate 40 ppm CO ) (5.13). During the evaluation of the Draeger Datalogger, it was noted high concentrations of the lower alcohols produced large positive biases when the monitor was exposed to headspace concentrations. Dataloggers were also placed near the open tops of glass bottles containing the chemicals listed below and monitor response was noted:

<u>Chemical</u>	<u>Response</u>	<u>Chemical</u>	<u>Response</u>
ethanol	positive	acetonitrile	no response
isobutanol	positive	acetone	response*
isopropanol	positive	butylamine	no response
methanol	positive	dimethylamine	no response
n-propanol	positive	ethyl acetate	no response
		formaldehyde	no response**
		isooctane	no response
		1-octanol	no response
		toluene	no response

\* Acetone gave a positive response when the CO-specific filter was removed or when the filter had diminished capacity (been in use over 1 year)

\*\* A 37% solution of formaldehyde gave a response which was primarily due to the 10 to 15% methanol used as a stabilizer. When formaldehyde was produced by heating paraformaldehyde (no methanol present), a response was not noted when the CO-specific filter was new. A positive response was noted to the formaldehyde vapors when the filter was removed or had diminished capacity.

The responses indicated lower alcohols gave positive responses and others structurally similar to CO (i.e. acetone) could give a response if the CO-specific filter is removed or the filter has diminished capacity. Placement of the monitors into atmospheres saturated with each substance giving a positive response gave very large false positive readings for CO and also tended to fatigue the sensor. In addition, fine mists or droplets of the positive-interfering substances will produce similar false positive results. These interferences were produced using near-saturated or saturated atmospheres and should not be significant at concentrations near the PELs for these compounds. Concentration estimates for those substances giving positive responses at saturated vapor conditions are shown in Appendix A (Note: These are only rough approximations). The industrial hygienist should note whenever there is a significant amount of these compounds present (i.e. some confined space monitoring may have near-saturated or saturated atmospheres), or operations where droplets or fine mists of these substances could contact the surface of the filter/sensor of the Datalogger. If large amounts or aerosols of these substances are expected, monitoring for the interfering substances should take precedence, and an alternate method such as OSHA Method No. ID-210 can be used for CO monitoring if necessary. *It is highly recommended that the CO-specific filters be changed periodically.*

Early reports from other Datalogger users indicated a positive bias was observed when the monitor was placed near liquid aerosol streams. To assess if small liquid droplets could trigger a positive reading, aerosols of water or ethyl acetate were sprayed directly above the monitor sensor and produced no response.

1.7. Physical Properties (5.15, 5.16) and CAS No.

CAS No. (Carbon Monoxide):	630-08-0
Molecular weight:	28.01
Molecular formula:	CO
Appearance:	Colorless, odorless gas
Explosive limits in air:	12.5 to 74.2% (v/v)
Autoignition temperature:	651 °C
Melting point:	-207 °C
Boiling point:	-191.3 °C
Specific gravity (air = 1):	0.968
Density, gas at 0°C, 101.3 kPa (760 mmHg):	1.25 g/L
Solubility	
at 0 °C:	3.54 mL/100 mL water
at 25 °C:	2.14 mL/100 mL water

1.8. Prevalence and Use of CO

With the single exception of CO<sub>2</sub>, the total yearly emissions of CO exceed all other atmospheric pollutants combined (5.16). Potential sources for CO emission and exposure are listed (5.16, 5.17):

- Foundries
- Petroleum refineries
  - Fluid catalytic crackers
  - Fluid coking operations
  - Moving-bed catalytic crackers
- Kraft pulp mills
- Carbon black manufacturers
- Steel mills
- Coke ovens
- Basic oxygen furnaces
- Sintering operations
- Formaldehyde manufacturers
- Coal combustion facilities
- Utility and large industrial boilers
- Commercial and domestic furnaces
- Fuel oil combustion operations
- Power plants
- Industrial, commercial, and domestic uses
- Charcoal manufacturers
- Meat smokehouses
- Sugarcane processing operations
- Motor vehicles

## 1.9. Toxicology

---

Note: Information contained within this section is a synopsis of the present knowledge of the physiological effects of CO and is not necessarily intended to be used as the basis for OSHA policy.

---

Carbon monoxide has over a 200-fold greater affinity for hemoglobin than has oxygen (5.18, 5.19). Thus, it can make hemoglobin incapable of carrying oxygen to the tissues. The presence of CO-hemoglobin (COHb) interferes with the dissociation of the remaining oxyhemoglobin, further depriving the tissues of oxygen (5.15, 5.16).

The signs and symptoms of CO poisoning include headache, nausea, weakness, dizziness, mental confusion, hallucinations, cyanosis, and depression of the S-T segment of an electrocardiogram. Although most injuries in survivors of CO poisoning occur to the central nervous system, it is likely that myocardial ischemia is the cause for many CO-induced deaths (5.18).

The uptake rate of CO by blood when air containing CO is breathed increases from 3 to 6 times between rest and heavy work. The uptake rate is also influenced by oxygen partial pressure and altitude (5.20).

Carbon monoxide can be removed through the lungs when CO-free air is breathed, with generally half of the CO being removed in 1 hour. Breathing of 100% oxygen removes CO quickly.

Acute poisoning from brief exposure to high concentrations rarely leads to permanent disability if recovery occurs. Chronic effects from repeated exposure to lower concentrations have been reported. These include visual and auditory disturbances and heart irregularities. Where poisoning has been long and severe, long-lasting mental and/or nerve damage has resulted (5.15).

The following table gives the levels of COHb in the blood which tend to form at equilibrium with various concentrations of CO in the air and the clinical effects observed (5.21):

Atmospheric CO (ppm) COHb in	Blood (%)	Symptoms
70	10	Shortness of breath upon vigorous exertion; possible tightness across the forehead.
120	20	Shortness of breath with moderate exertion; occasional headache with throbbing in the
220	30	Decided headache; irritability; easy fatiguability; disturbed judgment; possible dizziness; dimness of vision.
350-520	40-50	Headache; confusion; collapse; fainting upon exertion.
800-1220	60-70	Unconsciousness; intermittent convulsions; respiratory failure; death if exposure is prolonged.
1950	80	Rapidly fatal.

Adults (non-smokers) normally have about 1% COHb in the body. Cigarette smokers generally have blood levels of 2 to 10% COHb (5.20).

In examining the CO levels in an occupational environment, CO generated from tobacco smoking may need to be considered. These amounts may ordinarily be small, but when added to the amounts generated by occupational activities, may aggravate conditions from an already existing high concentration of CO (5.22, 5.23).

#### 1.10. Other Hazardous Properties

Carbon monoxide is flammable and can be a dangerous fire and explosion risk. The flammable limits in air range from 12 to 75% by volume (5.19).

## 2. Sampling

Note: A training videotape (Draeger part no. 4505202) is available from Draeger regarding Datalogger 190 use and data transfer.

### 2.1. Precautions

- 2.1.1. Be certain that the radio frequency shielding of the monitor is intact.
- 2.1.2. Attach the monitor to the worker in such a manner that it will not interfere with work performance or safety.
- 2.1.3. Follow all safety practices that apply to the work area being sampled.
- 2.1.4. If the *employee being monitored* is smoking a tobacco product during sampling, a positive contribution of CO from the tobacco combustion may occur for personal samples. Ask the employee to refrain from smoking during sampling so that only the occupational exposure is considered.

- 2.1.5. Describe the audible alarms to the employee, and instruct the employee on what to do if they occur. The alarm is normally set to a level slightly above the OSHA Ceiling Exposure Limit of 200 ppm CO.

---

Note: The Immediately Dangerous to Life and Health (IDLH) and the OSHA Instantaneous Limit are the same concentration, 1,500 ppm CO. The Datalogger discussed in this method is unable to measure above 999 ppm. If the Datalogger registers readings above 999 ppm, appropriate protective measures should be taken to safeguard those exposed. If necessary to document excursions above the IDLH or OSHA Instantaneous Limit, detector tubes listed in the OSHA Chemical Information File can be used provided measurements can be safely taken.

---

## 2.2. Equipment

- 2.2.1. CO Datalogger or other validated direct-reading device (For information on specific equipment needed with the Draeger Model 190 CO Datalogger, see Appendix B. For interferences, please see Section 1.6)
- 2.2.2. Gases for calibration:
- CO calibration gas
  - CO-free nitrogen or CO-free air

## 2.3. Sampling Procedure

- 2.3.1. See Appendix B regarding specific information on preparation, alarm adjustment, calibration, and other procedures for the Draeger Model 190 Datalogger.
- 2.3.2. Calibration - Use only certified calibration gases. For OSHA purposes, the recommended concentration of the calibration gas (span gas) is 30 to 70 ppm CO (listed to the nearest 0.1 ppm). Gas cylinders are available from the OCL (see Appendix C)(5.24). The gas cylinders can be mailed or expressed to the site from OCL using appropriate shipping procedures.

- 
- Notes:
1. Do not perform calibrations in the presence of an operating radio transmitter. Calibrate the monitors in a clean, well-ventilated environment; if possible, in a well-ventilated exhaust hood. Pre- and post-calibrate the monitors each time measurements are taken.
  2. In order to eliminate possible effects on calibration due to variations in altitude (pressure difference), calibrate the monitors at the same altitude at which they are to be used. Altitude corrections (calibrating at one altitude and taking measurements at another) were not investigated in this evaluation.
  3. Calibrate the monitors using the manufacturer-recommended flow rate of 0.20 L/min. Samples taken in areas of high air velocities (directed toward the monitor sensor) may indicate high CO readings. If necessary, gas bag samples can also be taken and submitted for laboratory analysis [use OSHA Method No. ID-210 (5.12)]. Air velocity does not have a significant effect on gas bag sample results.
  4. If possible, calibrate the monitors in the field. The effects of vibration during shipping have not been investigated.
-

2.3.3. General instructions - Sampling with a direct-reading instrument:

2.3.3.1. Start the monitor sampling. Record the time at the start of sampling.

2.3.3.2. Place the monitor in the breathing zone of the user, preferably secured or attached in a breast pocket. Be sure the sensor is not obstructed.

2.3.3.3. Sample for the time indicated:

a. TWA Determination: 8 h (if possible)

b. Ceiling Determination: 5 min - If datalogging is available in 5-min increments or less, a full-shift (8 h) sample can be taken and any overexposure to Ceilings can be determined as discussed below (Section 3.2).

2.3.3.4. Terminate sampling.

3. Data Recovery

3.1. Refer to instrument manuals and operating procedures for proper operation of all instruments. See Appendix B for information on the data recovery procedures for the Draeger Model 190 Datalogger.

3.2. Calculate Ceiling exposures if they are not calculated in 5-min increments by the instrument. Most commercially available instruments will measure in 1-min increments. Hand-calculate an average of 1-min segments for each 5-min Ceiling exposure. The 1-min increments must be consecutive.

3.3. Generate hard copies of the results. Show a display of the results and a graph.

3.4. Report the results as ppm CO.

4. Backup Report

Experimental Protocol

The evaluation of the instrument consisted of the following experimental protocol:

1. Analysis of the sample data from six Dataloggers exposed to dynamically generated CO atmospheres having concentration ranges of approximately 0.5, 1, and  $2 \times$  TWA PEL.
2. Evaluation at levels commonly encountered during IAQ investigations (approximately 5 and 10 ppm CO).
3. Evaluation at levels near the Ceiling PEL (approximately 200 ppm CO).
4. Determination of any variation in results when sampling at low and high humidity levels.
5. Assessment of any significant effect from varying the air flow rate over the monitor sensor during the evaluation tests.
6. Determination of the qualitative and quantitative detection limits for the analysis of CO.
7. Comparison of Datalogger results with a GC method (5.12) used for CO determinations in which the CO was analyzed using a GC-DID.
8. Assessment of the performance of this method and conclusions.

All results were statistically examined for outliers and, when necessary to pool results, homogeneous variance. Possible outliers were determined using the American Society for Testing and Materials

(ASTM) test for outliers (5.25). Homogeneity of the coefficients of variation was determined using the Bartlett's test (5.26). Overall Error was calculated as:

$$OE_i = \pm(|mean\ bias_i| + 2CV_i) \times 100\%$$

where i is the respective instrument pool being examined (5.27).

Six Dataloggers were used, and the statistical values for each set of determinations are based on the analysis of data consisting of one result from each of the six instruments.

This evaluation was split into two blocks of time [early work ("A" experiments) and later work ("B" experiments)].

4.1. Analysis - Because of the nature of the monitor and the data collection procedure, the sample spiking procedure normally performed during the evaluation of a sampling and analytical method was not possible; therefore, this experiment (analytical recovery,  $CV_1$ ) is not relevant to this direct-reading monitor.

4.2. Sampling and Analysis

**Procedure:** Three sets of samples (at 0.5, 1, and 2 × TWA PEL) were collected and evaluated. Samples taken at 5 and 10 ppm CO (50% RH) were also prepared and analyzed. Six Dataloggers were evaluated at each of these sampling conditions. Samples were collected according to the procedure listed below.

Block Diagram of the Laboratory Generation System

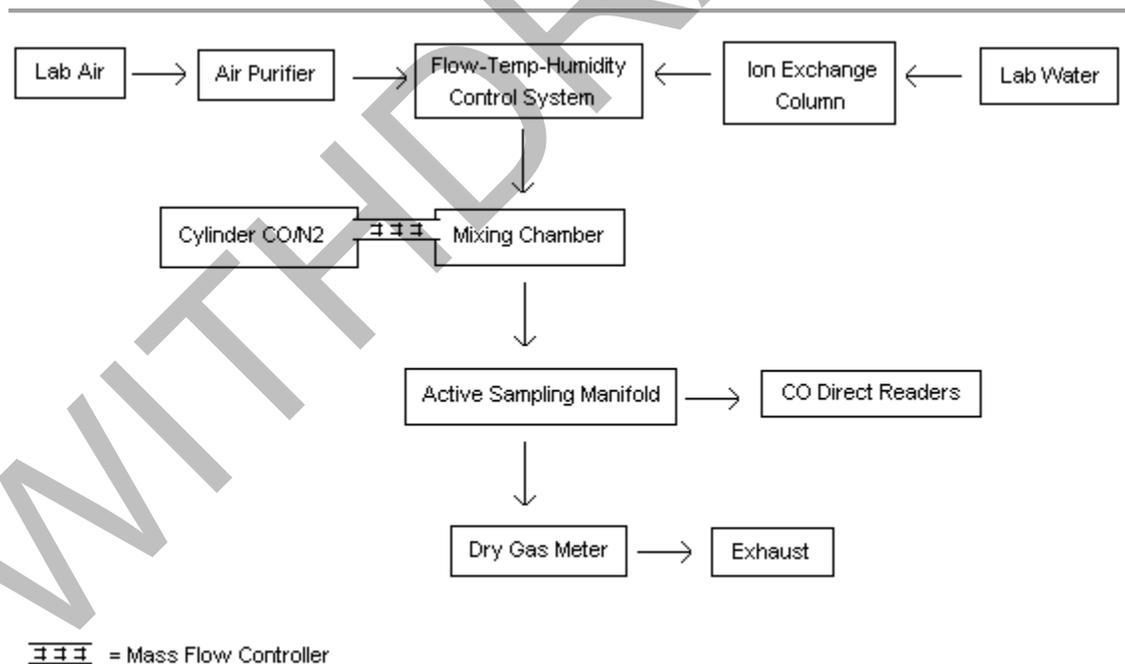


Figure 1a

4.2.1. A dynamic gas generation system was assembled as shown in Figure 1a. Moisture and other contaminants were removed from the diluent air by using a charcoal/Drierite/silica gel filtering system. A hopcalite filtering system was also used in part of the later work ("B" experiments) in an attempt to reduce any background CO concentration. A humidity,

temperature, and flow control system (Model HCS-301, Miller-Nelson Research Inc., Monterey, CA) was used to treat the diluent air to produce the stated RH at 25 °C. Diluent air flow was measured before and after each experiment using a dry test meter (DTM-115, American Meter Co., Philadelphia, PA). The flow control system had earlier been calibrated in-house for temperature and humidity. The Dataloggers were connected to the sampling manifold of the generation system using connectors (Figure 1b) similar to the one used for calibration. The free end of the Tygon® tubing was attached to a sampling manifold exit port (Teflon® tubing) for each Datalogger.

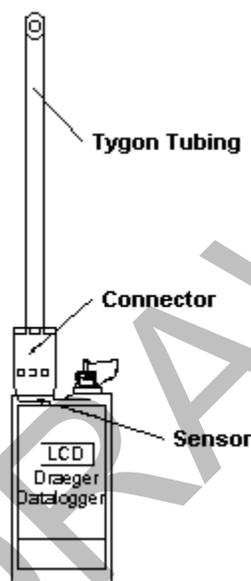


Figure 1b

For connectors, short pieces of rubber tubing slipped over rubber stoppers were drilled in the sides to allow test atmospheres moving down the Tygon® tubing to freely exit. The connectors were then used to attach the Datalogger sensor and Tygon tubing together. These connectors had slightly larger exit holes than the calibration units shown in Appendix B (Figure 8) to allow the generated atmosphere to freely pass over the sensor during testing. This type of sampling connection allowed the linear face velocity to be altered during testing. Passive monitor test chambers were used in additional experiments (Sections 4.4 and 4.6) without the use of connectors.

4.2.2. A gas cylinder containing approximately 0.5% CO in nitrogen was used as the CO source. For the "A" experiments, the gas was from Linde Div., Union Carbide Corp., Denver, CO (concentration certified at 0.50%). For the "B" experiments, the gas was from Airco, Riverton, NJ (certified at 0.496%). The CO was introduced into the flow system via a glass mixing chamber. Gas flow rates were controlled using a mass flow controller (Model FC-261, Tylan Corp., Torrance, CA). Gas flows were measured immediately before and after each experiment using a soap bubble flowmeter (Model 823-1, Mast Development Co., Davenport, IA).

4.2.3. To assure a continuous generation of controlled concentrations of CO and provide an additional verification of concentrations, the flow system was continuously monitored during each test by noting the LCD readings on the Dataloggers and, during the "A" experiments, with a direct-reading instrument [Model 7140 (for CO), Interscan Corp.,

Chatsworth, CA] connected to the flow system. Calibration of the Interscan direct-reading instrument was performed with a 40-ppm calibrating gas (CO in air, certified, Alphagaz, Cambridge, MD).

- 4.2.4. Calibration of the Dataloggers during the "A" experiments was performed with the 40-ppm calibrating gas mentioned above. Calibration during the "B" experiments was done using 104 ppm CO in nitrogen (certified, Airco, Inc., Murray Hill, NJ). The CO content of this cylinder had been confirmed in a previous study (5.12). For the "B" experiment calibrations, the gas flow over the face of each Datalogger was regulated with a regulator-rotameter system and the flow rates were measured using a soap bubble flowmeter (Model M-5, A. P. Buck, Inc., Orlando, FL).

---

Note: Preliminary experiments and a personal communication with the manufacturer indicated that the concentration of the calibration gas did not appear to have a significant effect on precision and accuracy as long as the calibration concentration was in the vicinity of the PEL. The manufacturer did state the higher calibration concentration (104 ppm CO) would probably give slightly more accurate results because of the greater linear range.

---

- 4.2.5. During the course of each "A" experiment, the monitors were calibrated and then attached to the generation system. The tempered CO/air mixture from the system was permitted to flow over the sensors and datalogging was initiated. At the conclusion of the experiment the logging was stopped and the monitors were removed from the system. The collected data were then downloaded to a computer.

For the "B" experiments a calibration was performed, then readings from the monitor LCDs were taken with only air flowing through the system. The CO flow was then started and, after stabilizing, datalogging was begun. At the conclusion of the experiment, datalogging was stopped, CO gas flow was stopped, monitor readings of the generation system air were again obtained, and then the monitors were removed from the system. (Note: A few problems occurred during the generations and are further discussed following the Results Section.)

**Results:** The results for generated samples at 0.5, 1, and 2 × PEL (50% RH) based on the TWA output values are listed in Table 1a. These represent Datalogger outputs [i.e., results are rounded down (truncated) to the next lower integer ppm value by the Datalogger]. The results for the generated samples based on the actual rounded hand-calculated average of all 1-min ppm values collected are listed in Table 1b. In principle, these hand-calculated results should represent a greater degree of accuracy because the truncation error is not present; however, the hand-calculated average is very tedious to determine. For CO levels in the region of the TWA PEL, the precision and accuracy results for the two calculation procedures were comparable.

The "A" experiments were conducted using calibration flow rates slightly higher than the recommended rate of 0.2 L/min. This would result in slightly lower Datalogger concentration readings during the "A" experiments. However, uncompensated background CO in the diluent air would result in a slightly larger generated CO concentration than the theoretical calculations. Thus, one source of error could have canceled the other.

The sampling and analysis data showed very good precision and accuracy. All data passed the outlier and Bartlett's tests; therefore, the data were pooled. The CV<sub>2</sub> (Pooled) value based on the TWA output values is 0.040 for samples taken in the range of 16 to 70 ppm CO (50% RH).

---

Note: Two problems were noted during the generations. These were sensor face velocity dependence, and background contamination during the "B" experiments.

Using the tubing devices similar in design to the Draeger calibration adapter to connect the Dataloggers to the sampling manifold of the generation system, it was found that increasing the flow rate of CO-containing air over the Datalogger sensor tended to result in higher CO concentration readings, even though the concentration had not changed. This was possibly due to a slight increase in pressure at the face of the sensor caused by the high gas flow rates through the connecting tubing. The pressure at each sampling port was estimated by a water manometer to be 2 to 6 mm water above the surrounding atmosphere. Flow rates used during the studies tended to be higher than the 0.20 L/min recommended for normal calibrating. Slight increases in CO recoveries possibly occurred due to increased pressure and not from humidity. This calibration flow rate dependence is further discussed in Section 4.6 For two of the "B" experiments (1 × PEL, 30% RH and 0.5 × PEL, 80% RH) an attempt was made to examine this effect by having significantly different gas flows when calibrating and taking the samples. The other "B" experiments were conducted by closely matching the calibration gas flow with the generation system flow.

Also during the "B" experiments, it was noted that significant background levels of CO existed in the laboratory atmosphere, in some cases up to 6 ppm. This was readily apparent when observing the Dataloggers' operation after zeroing the monitors with nitrogen. At the time of the "B" experiments, a climatic temperature inversion occurred, and higher than normal concentrations of CO were retained in the lower atmosphere. Because the diluent air is prepared from atmospheric air, this contamination could result in higher than normally expected CO concentrations in the generating system. Normal expected background CO concentrations in the generation system were <1 ppm. Prescrubbing the diluent air for the generation system through hopcalite removed only about one-half the amount of CO. With the hopcalite prescrubbing, the CO concentration was still occasionally observed to drift slightly as the experiment proceeded.

To compensate for the elevated CO background noted during the "B" experiments, "blank addition" was performed. The background CO concentration was determined by averaging a few monitor readings after the monitors were connected to the generation system with the dilution air passing over them (prior to 0.5% CO addition) and also at the conclusion of the experiment (after the 0.5% CO had been turned off). The average CO concentration determined from these readings was added to the theoretical concentration derived from the CO gas and diluent air flows to obtain a corrected theoretical concentration. These corrections ranged from 0.5 to 4 ppm CO.

---

#### 4.3. Sampling and Analysis at Low CO Levels

**Procedure:** In order to evaluate the Dataloggers at CO levels commonly encountered during IAQ investigations, test atmospheres at about 5 and 10 ppm CO (50% RH) were prepared and Datalogger samples were taken, using the same equipment and the sensor conditions described

in Section 4.2. The effects of the gas flow rate over the sensor, as well as the CO background concentration in the generator diluent air, were accounted for in these studies. Six Dataloggers were evaluated at each concentration.

**Results:** Recoveries for the samples generated at approximately 5 and 10 ppm CO are given in Table 2a (Datalogger truncated TWA output values) and Table 2b (hand-calculated averages of the 1-min ppm values collected by each Datalogger).

Results at 5 ppm gave a large OE value; however, this concentration level is very low in relation to the TWA PEL for CO. The hand-calculated results in Table 2b are an improvement over TWA output values given in Table 2a. This is to be expected because, at these low levels, recovery values based on hand calculating are taken to the nearest 0.1 ppm (Table 2b). The TWA output values (Table 2a) are truncated to the next lowest whole ppm.

#### 4.4. Sampling and Analysis at Ceiling CO Levels

**Procedure:** In order to evaluate the Dataloggers at CO levels in the vicinity of the Ceiling PEL (for a 5-min exposure period), generated samples near 200 ppm CO (50% RH) were also prepared and analyzed. For this experiment, six dataloggers were calibrated using the 40-ppm CO gas previously mentioned, and then mounted in a Du Pont gas flow chamber [E. I. Du Pont de Nemours and Co., Inc., Wilmington, DE. An excellent description of a similar chamber and the mixing chamber (Figure 1a) can be found in reference 5.28] designed for passive monitor evaluation. The chamber was connected to the generation system using Teflon tubing. The cross-sectional area in the chamber was 83.87 cm<sup>2</sup> (5.29). The gas flow rate in the chamber during the experiment was estimated by calculation as 1.1 m/min (3.6 ft/min). The experimental procedure consisted of placing the Dataloggers along a rigid Teflon tube in the chamber before assembling the system. The Dataloggers were mounted with the sensors facing upward, toward the direction of air flow through the chamber. Datalogging was initiated immediately before the monitors were mounted in the chamber. After placing the monitors in the chamber, air flow was started, then the 0.496% CO was turned on.

After the CO concentration in the chamber had stabilized (determined by observing the monitor LCDs through the glass chamber wall), two gas bag samples of the CO/air mixture were taken for GC analysis from a sampling manifold connected to the Du Pont chamber. At about 50 min after the CO concentration had stabilized, the gas flows were stopped and the Dataloggers were removed and datalogging was halted.

**Results:** Recoveries for the samples generated at approximately 200 ppm CO are given in Table 3. The hand-calculated averages of the 1-min ppm values collected by each Datalogger for the time period of interest were used. Results are given for:

1. the first 5-min period after the CO concentration readings began to stabilize, and
2. the entire period from when the CO concentration began to stabilize to the stopping of the CO flow. Calculated recoveries were 96.1% for the initial 5-min time period and 93.9% for the entire period. As previously stated in Sections 1.3, 1.4, and 3.2, the Datalogger system only gives 1-min averages and, therefore, 5-min truncated values are not displayed by the Dataloggers.

#### 4.5. Humidity Study

**Procedure:** Samples were also generated at 30% and 80% RH using the same equipment and conditions described in Section 4.2. An experiment was not conducted for 2 × TWA PEL at 30% RH.

**Results:** The results for the generated samples collected at the three RH levels are listed in the following Tables:

Table	% Humidity	Determination
1a	50	Truncated values
1b	50	Hand-calculated average values
4a	30	Truncated values
4b	30	Hand-calculated average values
5a	80	Truncated values
5b	80	Hand-calculated average values

Two "B" experiment tests (1 × PEL at 30% RH and 0.5 × PEL at 80% RH) showed a positive bias in the mean recoveries obtained. These were initial "B" experiments, and were conducted with calibration flow rates lower than generation system flow rates. The increased flow across the sensor face as compared to the calibration flow was suspected of causing the higher bias.

As shown in Table 6, an analysis of variance (F test) (5.30) was performed on the data to determine any significant difference among or within the various RH groups. Variance at each concentration (0.5, 1, and 2 × TWA PEL) was compared across the three RH levels (30%, 50%, and 80% RH). The variance among and within the different concentration groups gave high calculated F values at 0.5 and 1 × PEL. The large calculated F values appear to be mainly due to variability in mean recoveries, and are most likely related to variance from sensor face velocity differences within the experiments.

Recalculation of F values after making estimated corrections for face velocity differences between calibrations and generation system measurements reduced the F values considerably.

#### 4.6. Assessment of the Rate of Gas Flow on the Datalogger Readings

**Procedure:** As mentioned previously in Section 4.2.1, tubing devices similar to the Draeger calibration adapter were used to connect the Dataloggers to the generation system. Under these conditions, generation system flow rates over the Datalogger sensor faces (linear face velocities) tended to be high, and therefore, higher CO sample concentration readings were obtained.

An investigation of face velocity dependence of gas flowing through the calibration adapter or similar tubing was conducted with six Dataloggers which were calibrated with the 104-ppm CO certified standard mentioned in Section 4.2.4. Four different sets of tests were conducted:

1. Two tests were performed to determine linear face velocity effects on Datalogger readings; in one experiment the Dataloggers were calibrated with the gas flow set at 0.60 L/min, and in the other the calibration was conducted with the gas flow set at 0.20 L/min. In each experiment, readings were then taken from the Dataloggers as the rate of flow of the 104-ppm CO through the calibration adapter over the sensors was varied.
2. In a test using three monitors, the tubing similar to the calibration device was replaced with a short piece of glass tubing which fit loosely over the monitor sensor cap. Gas flows ranging from 0.20 to 2.50 L/min were permitted to flow over the sensors.
3. A test was conducted to determine any effect of varying the nitrogen flow over the sensor after zeroing the monitor. The monitors were zeroed and then the flow rate of pure nitrogen

was increased while attached to a Datalogger. Any change from a zero reading in the Datalogger output was noted.

4. A test was conducted to evaluate the effect of fast (turbulent) air flow past the Datalogger sensors when the monitors were surrounded by the moving air, rather than being exposed only through the adapter tubing over the sensor (linear flow). Four Dataloggers were exposed in a chamber to air containing 102 ppm CO at 50% RH derived from the generation system. In the chamber, the air was stirred with a fan so that turbulent air at speeds of 15.2 to 91.4 m/min (50 to 300 ft/min) could be swept by the monitors and their sensors.

**Results:** For test (1), the Datalogger readings as a function of gas flow across the face of the sensor (face velocity) are given in Figure 2. It is evident that the readings tend to rise as the linear flow increases, and a "steady state" is achieved where the readings stop rising at a certain point.

Datalogger Readings vs. Flow Rate

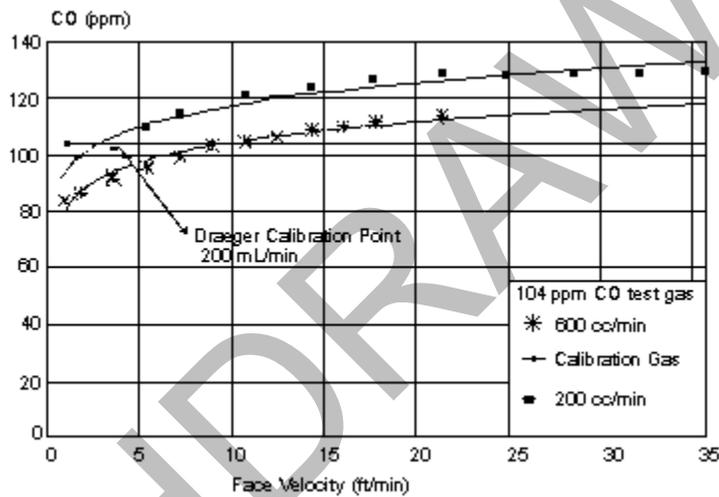


Figure 2

Gas flow rates over the sensor in metric units are given below.

### Gas Flow Rate Over Sensor

L/min	m/min*	ft/min
0.0532	0.29	0.9
0.103	0.56	1.8
0.201	1.09	3.6
0.303	1.65	5.4
0.405	2.20	7.2
0.506	2.75	9.0
0.599	3.26	10.7
0.700	3.81	12.5
0.805	4.38	14.4
0.903	4.91	16.1
1.006	5.47	17.9
1.206	6.56	21.5
1.402	7.62	25.0
1.610	8.75	28.7
1.804	9.81	32.2
2.002	10.89	35.7

\* Based on a measured sensor exposure area of 1.839 cm<sup>2</sup>

For test (2) the rise in observed readings was less pronounced when tubing similar to the calibration tubing was replaced with the loose-fitting glass tube. It should be stressed in either test, the flow of the CO/air mixture is being applied directly at the sensors.

The Datalogger dependence on face velocity appears important during calibrations and appears partially due to increased pressure on the sensor face. Although the curvature shown in Figure 2 is important during calibration, it follows a similar pattern noted with other passive monitors. Face velocity dependence has been noted previously (5.29), and it is not unusual for a monitor to have:

- a. a very low sampling rate at low face velocities (<5-10 ft/min),
- b. a relatively constant ("steady state") sampling rate over a specific sampling range,
- c. a higher sampling rate at very large face velocities (>500 ft/min).

This effect of air flow rate on the results for passive monitors has been discussed further in a report from the National Institute for Occupational Safety and Health (5.31). Typical face velocities in general industry, according to the NIOSH report (5.31) are 10 to 150 cm/s (approximately 6 to 90 m/min or 20 to 300 ft/min).

In test (3) where the nitrogen flow after zeroing was altered, there was no significant change from zero as the flow rate of nitrogen increased. This indicates that pressure alone is not responsible for the elevated readings noted in tests (1) and (2).

In test (4) where the monitors were exposed to the rapidly moving turbulent air, the monitor readings leveled off in the range of 103 to 114 ppm CO. *The readings were similar even when*

*the fan was turned off. It appears the monitors are only slightly affected by turbulent air flows of 15.2 to 91.4 m/min (50 to 300 ft/min) where a positive bias of approximately 5 to 10% was noted. The monitor appears more affected by linear flows. It is expected in many industrial settings the air flow will move in a turbulent fashion.*

The manufacturer has reported the following calibration flow deviations when CO-containing gas flow rates different from the recommended 0.20 L/min are used:

ft/min	L/min	% Error
2.7	0.17	-8
2.9	0.18	-7
3.3	0.21	<3
3.7	0.23	<3

These manufacturer-determined values appear similar to those shown in Figure 2. The flows are clustered close to the recommended calibration flow rate of 0.2 L/min. According to the manufacturer, experiments in which the air velocity was varied from 0 to 6 m/s (1,200 ft/min), the sensitivity was  $\pm 5\%$  of the measured value (5.32). It is not known whether the test was conducted using linear or turbulent flows.

Both series of internal and manufacturer-performed experiments discussed above demonstrate a significant relationship of Datalogger accuracy and calibration flow rate. Significantly different results may be obtained during sampling if the Datalogger is calibrated at flow rates different than recommended (0.2 L/min).

#### 4.7. Detection Limits

**Procedure:** Both qualitative and quantitative limits for the analysis of CO by the Dataloggers were calculated using the International Union of Pure and Applied Chemistry (IUPAC) method for detection limit determinations (5.33). The data collected at 50% RH and 5.6, 11.1, and 16.1 ppm (Tables 1a, 1b, 2a, and 2b) were used. Also included were data from a blank generation in which no CO was added. The blank generation was performed when the background CO level in the air was at a very low level (0 to 1 ppm).

**Results:** The detection limit results are listed in Table 8a (for the truncated TWA output values) and Table 8b (for the hand-calculated averages of all of the 1-min ppm values). A derivation of the IUPAC method was used for the data in Table 8a because the blank readings were zero. The standard deviation of the lowest concentration standard was used in place of the blank for data in Table 8a. The results are summarized as follows:

Detection Limit	Truncated TWA Values	Hand-Calc. Ave of 1-min
Qualitative:	1.2 ppm	0.5 ppm
Quantitative:	4.1 ppm	-1.8 ppm

The lower detection limits for the "Hand-Calc. Ave." of all the 1-min ppm values is to be expected, since fractional values for the ppm determination are calculated, averaged, and rounded. This type of data (rounded rather than truncated) is also more attuned to the gaussian statistical model used. Also, hand-calculated averages are indicative of the ultimate CO measuring capabilities of the instrument at low concentrations.

#### 4.8. Comparison of Methods

**Procedure:** In order to confirm the accuracy of the CO concentration of the 0.50% and 0.496% CO sources used in the generation system, as well as the accuracy of generation, one or two gas bag samples were taken from the generated gas stream during each Datalogger study. Bags employed were 5-L five-layer aluminized gas bags (Calibrated Instruments, Inc., Ardsley, NY). Analysis of the CO content of the gas bags was performed with a Tracor Model No. 540 GC equipped with a Model No. 706 DID according to OSHA Method ID-210 (5.12). Standards were prepared from the cylinder of 104-ppm CO in nitrogen previously discussed in Section 4.2.4.

The CO concentration of this gas cylinder had been confirmed during previous work by reaction with iodine pentoxide and titration of the subsequent iodine produced (5.12).

**Results:** The GC results were compared with theoretical values (e.g., "GC Results" = GC Recovery/Theoretical Value). Theoretical values were calculated from generation system flow settings. As shown in Figures 3 - 5, good agreement is noted between theoretical and GC results. The Datalogger results ("Datalogger" = TWA Output Values, Calc Average = Hand-Calculated Average Values) are also illustrated for comparison purposes. It should be noted in Figure 4 the TWA output value (Datalogger result) for the Ceiling determination is not present. In this case the results were hand-calculated as previously mentioned in Section 4.4.

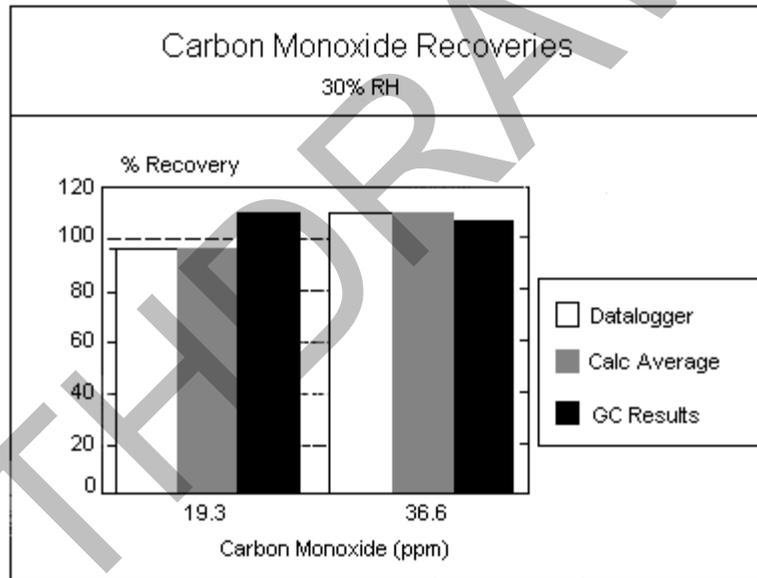


Figure 3

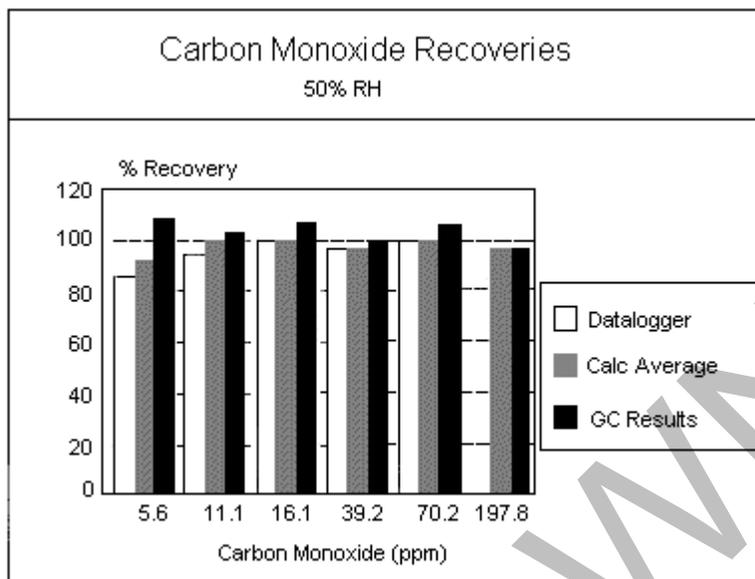


Figure 4

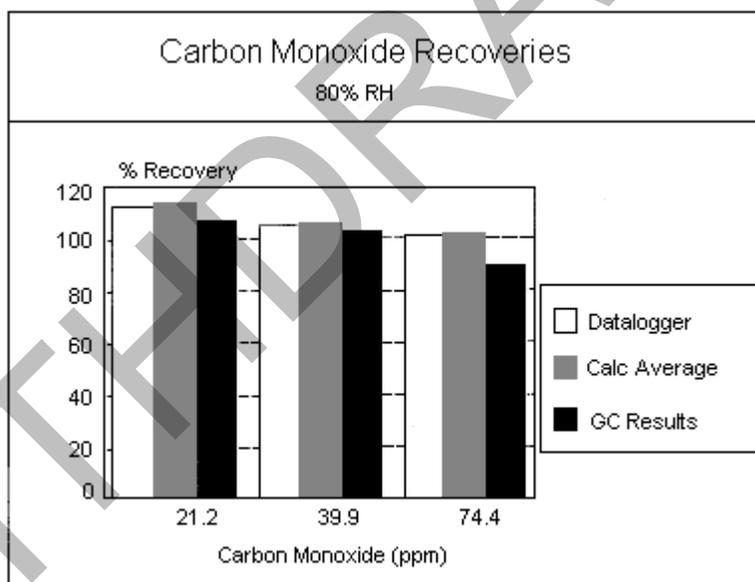


Figure 5

#### 4.9. Conclusions

The experimental results indicate this direct-reading monitor is an excellent means for sampling and analyzing CO in the workplace if properly calibrated and if air flow is not directly at the face of the monitor sensor (linear flow). Obtaining accurate analytical results for other-than-normal conditions existing in the working environment may be contingent on matching the flow of the calibration gas. Although the precision and accuracy results were still acceptable when the calibration/generation system flow ratios were different by a factor of two (Tables 4a and 5a), the monitors should normally be calibrated using the manufacturer-stated flow settings. If the face velocity in the sampling environment simulates a linear flow (i.e. measurements inside of air ducts), calibration flow can be matched to sampling flows to provide for more accurate results. It

should be noted that turbulent flow at the face of the sensors did not produce the magnitude of positive bias noted to occur during the linear face velocity tests. The positive bias is likely partially due to increased pressure on the CO sample directly above the sensor face. The Dataloggers should be calibrated at the same altitude as the site where sampling will be conducted.

Because the instrument automatically performs integer math for calculations (truncating to the next lower integer ppm value), rounding-off error for the resulting TWA output values is possible. This does not appear problematic for CO concentrations normally encountered in industry, and is aptly shown by comparable precision and accuracy data obtained when testing in the vicinity of the PEL (Tables 1a and 1b). The error does become significant at single digit levels (i.e., <10 ppm); however, these levels are well under the present TWA PEL. It should also be pointed out that in workplace environments the CO level will not be static and may quite often rise to high concentrations and fall to single digit values in one monitoring period.

Determinations near the TWA PEL were well within NIOSH and OSHA accuracy and precision guidelines (5.26, 5.27). For the truncated TWA output values at 50% RH, the pooled coefficient of variation (CV<sub>2</sub>) was 0.040 and the overall recovery was 98.4%. An effect from humidity is not apparent. In two cases where the OE values appear somewhat high (1 × PEL at 30% RH and 0.5 × PEL at 80% RH), face velocity and increased pressure at the sensor face appear as contributory factors. The manufacturer of the Datalogger may need to further investigate interferences caused by low molecular weight alcohols and aldehydes which appear structurally similar to the CO molecule. These interferences are not expected to be significant in normal workplace monitoring but may cause problems during confined space evaluations.

The OE values at approximately 5 and 10 ppm CO were somewhat high, but within NIOSH and OSHA guidelines if non-truncated values are used.

The Dataloggers are very convenient to use. There is minimum interference with work procedures by employees. The exposure data are stored and easily recovered to produce a minute-by-minute record of the working environment.

This sampling and analytical method is capable of accurate and precise measurements to determine compliance with the 35 ppm TWA or 200 ppm Ceiling PEL for CO exposures.

## 5. References

- 5.1. "Air Contaminants; Final Rule" Federal Register 29 CFR Part 1910 (19 Jan. 1989). pp. 2332-2983.
- 5.2. United States Department of Labor, OSHA: "Memorandum, Updated Changes to 29 CFR 1910.1000, Air Contaminants Standard." by Patricia Clark, Director Designate, Directorate of Compliance Programs. United States Department of Labor, OSHA, Washington, DC, June 1, 1990. [Memo].
- 5.3. "Air Contaminants; Corrections" Federal Register 29 CFR Part 1910 (1 July 1992). pp. 29204-29206.
- 5.4. Occupational Safety and Health Administration Salt Lake Technical Center: Chemical Information File, Online Database-OSHA Information System. Salt Lake City, UT: Occupational Safety and Health Administration Salt Lake Technical Center, 1989.
- 5.5. Katz, M., ed.: Methods of Air Sampling and Analysis. 2nd ed., APHA Intersociety Committee. Washington, D.C.: Publication Office, American Public Health Association, 1977. No. 132, pp. 368-369.

- 5.6. Occupational Safety and Health Administration Salt Lake Technical Center: Carbon Monoxide Detector Tubes (Short-Term) (USDOL/OSHA-SLTC PE-11). Salt Lake City, UT: Occupational Safety and Health Administration Salt Lake Technical Center, 1990.
- 5.7. Occupational Safety and Health Administration Salt Lake Technical Center: A Laboratory Evaluation of Draeger Long Duration Carbon Monoxide Detector Tubes (USDOL/OSHA-SLTC PE-3). Salt Lake City, UT: Occupational Safety and Health Administration Salt Lake Technical Center, 1981.
- 5.8. National Institute for Occupational Safety and Health: NIOSH Manual of Analytical Methods. 2nd. ed., Vol. 1 (Method No. P&CAM 112) (DHEW/NIOSH Pub. No. 77-157-A). Cincinnati, OH: National Institute for Occupational Safety and Health, 1977.
- 5.9. National Institute for Occupational Safety and Health: NIOSH Manual of Analytical Methods. 2nd. ed., Vol. 4 (Method No. S340) (DHEW/NIOSH Pub. No. 78-175). Cincinnati, OH: National Institute for Occupational Safety and Health, 1978.
- 5.10. Mine Safety and Health Administration: Regular Mine Gas Analysis (MSHA Standard Method No. 1). Denver, CO: MSHA, 1979.
- 5.11. Williams, D.M.: "Unique Applications for New Helium Glow Discharge Ionization Detector for Gas Chromatography." Paper presented at the 1988 Pittsburgh Conference, New Orleans, LA, February 1988.
- 5.12. Occupational Safety and Health Administration Salt Lake Technical Center: Carbon Monoxide in Workplace Atmospheres (USDOL/OSHA-SLTC Method No. ID-210). Salt Lake City, UT: Occupational Safety and Health Administration Technical Center, 1991.
- 5.13. National Draeger, Inc.: Draeger Model 190 Datalogger, CO, Operating Manual. Pittsburgh, PA: National Draeger, Inc., No date specified.
- 5.14. American Society of Heating, Refrigerating and Air-Conditioning Engineers Inc.: Ventilation for Acceptable Indoor Air Quality. ASHRAE 62-1989. Atlanta, GA: American Society of Heating, Refrigerating and Air-Conditioning Engineers, 1989. pp. 1-26.
- 5.15. Sax, N.I.: Dangerous Properties of Industrial Materials. 4th ed. New York: Van Nostrand Reinhold Company, 1975. pp. 520-521.
- 5.16. National Institute for Occupational Safety and Health: Criteria for a Recommended Standard-Occupational Exposure to Carbon Monoxide (DHEW/NIOSH Pub. HSM 73-11000). Cincinnati, OH: National Institute for Occupational Safety and Health, 1972.
- 5.17. Coburn, R.F., Chairman: Carbon Monoxide. Washington, DC: National Academy of Sciences, 1977.
- 5.18. Proctor, N.H. and J.P. Hughes: Chemical Hazards of the Workplace. Philadelphia, PA: J.B. Lippincott Co., 1978. pp. 151-153.
- 5.19. Sax, N.I. and R.J. Lewis, Sr.: Hawley's Condensed Chemical Dictionary. 11th ed. New York: Van Nostrand Reinhold Co., 1987. pp. 221-222.
- 5.20. American Conference of Governmental Industrial Hygienists: Documentation of the Threshold Limit Values for Substances in Workroom Air. 3rd ed. Cincinnati, OH: American Conference of Governmental Industrial Hygienists, 1971. pp. 41-43.
- 5.21. Ellenhorn, M.J., and D.G. Barceloux: Medical Toxicology. New York, NY: Elsevier Science Publishing Co., Inc., 1988. p. 821.

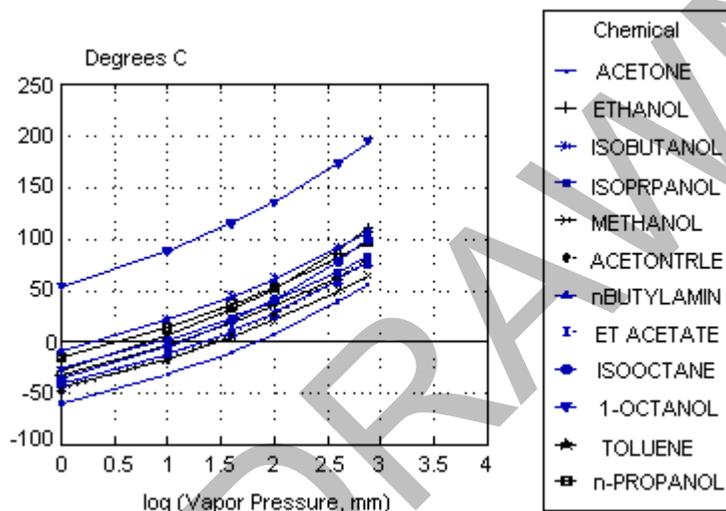
- 5.22. Lee, H.K., T.A. McKenna, L.N. Renton, and J. Kirkbride: Impact of a New Smoking Policy on Office Air Quality. In *Indoor Air Quality in Cold Climates: Hazards and Abatement Measures*, edited by D.S. Walkinshaw. Pittsburgh, PA: Air Pollution Control Association, 1986. pp. 307-322. (NIOSH-00172085).
- 5.23. Leaderer, B.P., W.S. Cain, R. Isseroff, and L.G. Berglund: Ventilation Requirements in Buildings. II. Particulate Matter and Carbon Monoxide from Cigarette Smoking. *Atmospheric Environment* 18, No. 1: 99-106 (1984). (NIOSH-00137853).
- 5.24. U.S. Department of Labor - OSHA: "Additions to Supplies Furnished by OCL, Memorandum for Regional Administrators, Area Directors, ARA's for Technical Support, Health Response Team." by Robert T. Williams. U.S. Department of Labor - OSHA, Cincinnati Laboratory, Cincinnati, OH, May 8, 1992. [Memo].
- 5.25. Mandel, J.: Accuracy and Precision, Evaluation and Interpretation of Analytical Results, The Treatment of Outliers. In *Treatise On Analytical Chemistry*. 2nd ed., Vol. 1, edited by I.M. Kolthoff and P.J. Elving. New York, NY: John Wiley and Sons, 1978. pp. 282-285.
- 5.26. National Institute for Occupational Safety and Health: Documentation of the NIOSH Validation Tests by D. Taylor, R. Kupel and J. Bryant (DHEW/NIOSH Pub. No. 77-185). Cincinnati, OH: National Institute for Occupational Safety and Health, 1977. pp. 1-12.
- 5.27. Occupational Safety and Health Administration Salt Lake Technical Center: OSHA Analytical Methods Manual. Vol. III (USDOL/OSHA-SLTC Method Validation Guidelines). Cincinnati, OH: American Conference of Governmental Industrial Hygienists (Pub. No. ISBN: 0-936712-66-X), 1985.
- 5.28. Freeland, L.T.: An industrial hygiene calibration manifold. *AIHAJ* 38: 712-720 (1977).
- 5.29. Occupational Safety and Health Administration Salt Lake Technical Center: Evaluation of a Solid Sorbent Passive Dosimeter for Collecting Mercury Vapor (USDOL/OSHA-SLTC Backup Report No. ID-140). Salt Lake City, UT: Occupational Safety and Health Administration Technical Center, revised 1989.
- 5.30. Dowdy, S. and S. Wearden: *Statistics for Research*. New York: John Wiley and Sons, 1983. Chapter 8.
- 5.31. Cassinelli, M.E., R.D. Hull, J.V. Crable, and A.W. Teass (National Institute for Occupational Safety And Health): Protocol for the Evaluation of Passive Monitors. In *Diffusive Sampling - An Alternative Approach to Workplace Air Monitoring, The Proceedings of an International Symposium held in Luxembourg, 22-26 September 1986*, edited by A. Berlin, R.H. Brown, and K.J. Saunders. London: The Royal Society of Chemistry, Burlington House, 1987. pp. 190-202.
- 5.32. Nancy Hoblack: "Effect of Air Velocity on Draeger CO Datalogger Readings." July 9, 1992. [Private Communication]. Nancy Hoblack, National Draeger, Inc., 101 Technology Drive, Pittsburgh, PA 15230.
- 5.33. Long, G.L. and J.D. Winefordner: Limit of Detection - A Closer Look at the IUPAC Definition. *Anal. Chem.* 55: 712A-724A (1983).
- 5.34. National Draeger, Inc.: *Enhanced Graphics Software (Version 1.0), Operating Manual*. Pittsburgh, PA: National Draeger, Inc.
- 5.35. U.S. Department of Labor - OSHA: "National Draeger CO Dosimeters, Memorandum for Rick Cee." by Robert T. Williams. U.S. Department of Labor - OSHA, Cincinnati Laboratory, Cincinnati, OH, February 7, 1991. [Memo].

## Appendix A

### Estimates of Saturated Vapor Concentrations of Selected Interferences

The saturated vapor concentrations for interferences discussed in Section 1.6 of this method were estimated from commonly found vapor pressure data. Six values for the temperature versus vapor pressure were given for each compound (the vapor pressure values were taken from the following reference: Lide, David R., ed.: CRC Handbook of Chemistry and Physics. 73rd ed. Boca Raton, FL: CRC Press, 1992-1993. pp. 6-68 to 6-82). These values were plotted for each compound of interest. The temperature in °C versus the logarithm of the vapor pressure was plotted as shown below:

Temperature vs log (Vapor Pressure)



The vapor pressures listed below at 25 °C were determined by interpolation. The saturated vapor concentration was then calculated using the equation:

$$\text{concentration} = \text{vp} \times 10^6 / P$$

Where: vp = vapor pressure and P = atmospheric pressure.

The tests were performed at an atmospheric pressure of approximately 650 mmHg. These are estimates of the concentration near the surface of the liquid; in practice, the Datalogger was held a short distance away from the liquid surface. The actual concentration of each substance during interference measurements was less than reported here.

Name	Vapor Pressure (mmHg)	ppm @760 mmHg	ppm @650 mmHg
Acetone	223.9	295,000	344,000
Ethanol	57.5	75,700	88,500
Isobutanol	12.6	16,600	19,400
Isopropanol	43.7	57,500	67,200
Methanol	123.0	162,000	189,000
Acetonitrile	91.2	120,000	140,000
n-Butylamine*	85.1	112,000	131,000
Ethyl acetate	93.3	123,000	144,000
Isooctane**	50.1	65,900	77,100
1-Octanol	0.1***	130	150
Toluene	28.2	37,100	43,400
n-propanol	20.4	26,800	31,400

\* Vapor pressures estimated from boiling temp. of 77.8 °C and vapor properties of related amines.

\*\* 2,2,4-trimethylpentane

\*\*\* Value estimated by extrapolation.

Two of the compounds tested for interferences with the Draeger Dataloggers were available only in diluted solutions. These were:

Formaldehyde, 37% wt/wt in water, with 10-15% methanol (preservative).

Dimethylamine, 26% wt/vol in water.

Values for the partial pressures of formaldehyde over its aqueous solutions as a function of temperature and solution concentration were obtained from the following reference:

Walker, J. Frederick: Formaldehyde. American Chemical Society Monograph Series #120. New York: Reinhold Publishing Corp., 1953. p. 92.

For 36.2 g formaldehyde/100 g water at 20 °C, the partial pressure of formaldehyde was given as 1.025 mmHg.

Name	Partial Pressure (mmHg)	ppm @760 mmHg	ppm @650 mmHg
Formaldehyde	1.025	1,350	1,580

This value is for HCHO in pure water, whereas the solution available in the laboratory also contained methanol. No attempt was made to estimate the partial pressure of the dimethylamine over its solution.

## Appendix B

### Equipment, Initial Preparation, Calibration, Sampling, and Data Recovery Procedures

#### Draeger Model 190 CO Datalogger (5.13, 5.34)

#### 1. Equipment

##### 1.1. Draeger Model 190 CO Datalogger (Figure 6)

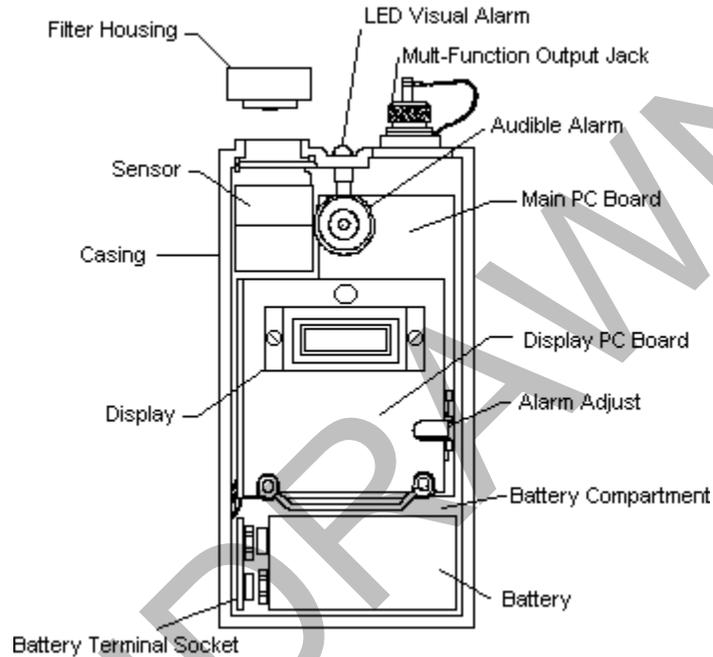


Figure 6

##### 1.2. CO-specific filter (filter housing in Figure 6)

##### 1.3. Red and blue function keys for starting and ending of datalogging (Figure 7)

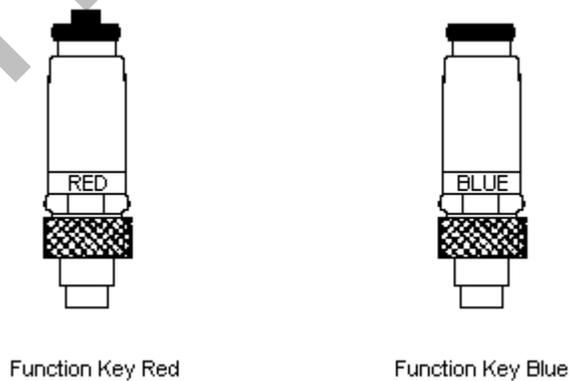


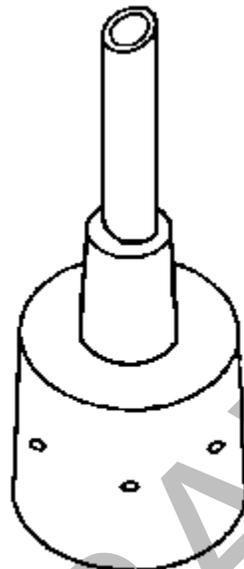
Figure 7

##### 1.4. Alkaline battery (9 volt)

##### 1.5. A small screwdriver for adjusting the zero, span, and alarm trim pots

##### 1.6. Calibration equipment and supplies

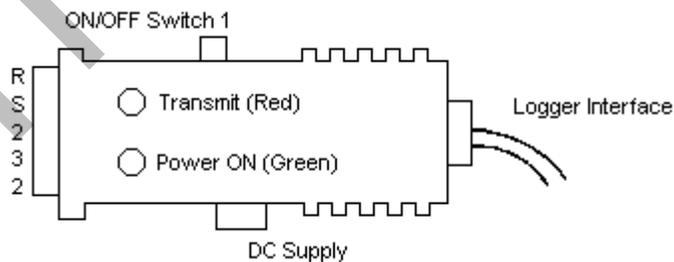
- 1.6.1. Calibration cylinder gas flow regulator (set to 0.20 L/min) (available from Draeger)
- 1.6.2. Calibration adapter (unit consisting of tubing attached to a perforated cap that fits over the monitor detection cell filter, see Figure 8)



Calibration Adaptor

Figure 8

- 1.6.3. Gas cylinder with certified CO concentration for calibration
- 1.7. Data reduction equipment
  - 1.7.1. Draeger RS-232 Interface, consisting of a Converter Box (25 pin) and Converter Box Power Supply for transferring the data from the Datalogger to a computer (Figure 9)



Converter Box

Figure 9

- 1.7.2. Computer program [National Draeger Inc. Enhanced Graphic Software (EGS) 2.0 Part Number 4510259] on a 32-in. (720K byte) micro diskette or a 5¼-in. (360K byte) disk

---

Note: These versions will not transfer data compatible to standard laser printers. Dot matrix printers shall be used unless the laser printer is modified for output. Contact Draeger for additional information.

---

- 1.7.3. MS-DOS operating system (Draeger did not stipulate in their documentation what version of DOS is required; however, DOS 3.3 and above appear compatible)
- 1.7.4. Computer such as an IBM or compatible AT or XT computer with an RS-232 (serial) port (Toshiba T1100PLUS Lap Top Computer)
- 1.7.5. Printer such as an IBM/Dotmatrix printer (Epson FX-86e).

## 2. Initial Preparation

- 2.1. Battery installation - Remove the battery cover by loosening the two screws and lifting off the cover. Insert a fresh 9-volt *alkaline* battery into the battery compartment and connect the battery terminal socket. The liquid crystal reading initially is a very high value and the alarm may activate. As the reading drops, eventually the alarm should become silent. Replace the battery housing; ensure that the battery lead wires will not be caught in between the covers. Seat the cover properly before the screws are tightened. Usually, a battery will last for about 1 month. If the Datalogger is not to be used for an extended period of time, the battery should be removed.

---

**Caution:** Do not replace the battery in potentially hazardous environments where a spark might cause an explosion.

---

- 2.2. Stabilization - When the battery is installed or a new unit is placed in service, a 24-h stabilization period is necessary. If the battery is only being replaced and the old battery indicates a low battery condition (by a short audible tone emitted about every 10 s, or an unstable LCD reading), allow a 2-h period for stabilization. Carefully install the blue key to reset the memory.

---

### Precautions

1. When installing the red or blue function keys, turn only the knurled ring at the base of the key. Do not attempt to twist the entire key, as the electrical prongs can bend excessively.
2. Replace the filter unit if it has become contaminated or has a large amount of trapped dust present.
3. After prolonged use, the electrochemical sensor may also need to be replaced, as evidenced by erratic behavior of the values observed on the LCD.

Note: The sensor contains sulfuric acid. Normally, use of the sensor does not result in exposure; however, if the container leaks or breaks, contact with the solution can cause severe burns or eye damage. If contact with the solution occurs, flush exposed body parts with cold water for about 10 min and get immediate medical attention.

---

- 2.3. Alarm adjustment procedure

---

### Precautions

1. If part of the circuit board remains under the edge of the cover after alarm adjustment, the cover will not be completely closed and the Datalogger will not be adequately shielded from radio frequency (RF) radiation. Loss of RF shielding can result in false readings and alarms if subjected to strong RF fields (5.35).

2. The alarm set point adjustment must be done in a clean air environment to avoid false zero adjustment levels.

---

Remove the filter unit from the monitor sensor. Loosen the three screws (located on the back side from the front panel) holding the housing cover in place and remove the cover. Locate the zero and alarm potentiometer adjustment screws (the alarm adjustment screw is between the zero and span adjustment screws, marked "Z" and "S" respectively). Adjust the zero potentiometer until the display indicates the ppm value of the desired alarm set point. [For compliance data collection, the alarm should be set to above 200 ppm CO (the Ceiling concentration value)]. If the alarm is sounding at concentrations lower than these, adjust the alarm set potentiometer clockwise until the alarm is silenced, then set counterclockwise until the alarm sounds. If the alarm is quiet at this concentration, adjust the alarm set potentiometer counterclockwise until the alarm sounds. Reset the zero potentiometer ("Z") to 0. Replace the housing. Be sure the battery lead wires are routed around the screw post. Tighten the three screws. Be sure the instrument circuit board in the upper chamber is properly seated and the housing is properly in place before the screws are tightened. Replace the dust filter.

### 3. Calibration

- 3.1. According to the manufacturer, "calibration must be performed at least on a monthly basis to keep the Model 190 Datalogger within published specifications" (5.13); however, for OSHA enforcement purposes, calibrate each time the monitors are used.
- 3.2. The recommended concentration of the calibration gas (span gas) should be 30 to 40 ppm CO. If necessary, higher concentrations of CO, 100 ppm or more, may also be used for calibration of the Draeger Dataloggers.

---

Note: The combination of the truncation feature of the Draeger Datalogger and the recommendation that the calibration gas should be 30 to 70 ppm CO increases the potential systematic error up to 3%. Using calibration gases whose concentrations are close to integer values (i.e. 39 ppm versus 39.8 ppm) will reduce this potential error.

---

- 3.3. Zero adjustment - Remove the blue function key, install the red function key and push the button on the key to stop the logging mode. Zero the instrument using the calibration adapter (see 1.6.2. above) and a source of CO-free nitrogen or CO-free air. Allow the nitrogen or air to flow at about 0.20 L/min until the reading stabilizes. Locate the zero adjustment screw ("Z"). Adjust the zero potentiometer until the display reads zero ppm CO. (Be certain that the potentiometer is capable of being adjusted to within  $\pm 5$  ppm.)
- 3.4. Calibration procedure (Span adjustment) - IF POSSIBLE, PERFORM THIS PROCEDURE IN A WELL VENTILATED AREA SUCH AS AN EXHAUST HOOD. Attach the monitor calibration adapter to the regulator on the calibration gas cylinder. Turn on the regulator (set to a flow rate of 0.20 L/min) and purge the calibration adapter. Place the calibration adapter over the filter housing. Wait until the LCD gives a constant reading. (New sensors may take more than 2 min to stabilize.) Locate the span adjustment screw ("S") on the side of the instrument. Adjust the span potentiometer until the display indicates the ppm value of the known calibration (span) gas (rounded to the nearest whole ppm).

---

Note: Do not perform calibrations in the presence of an operating radio transmitter.

---

#### 4. Sampling Procedure

- 4.1. The unit is ready for use when the battery is installed. Sufficient battery power is indicated by a periodic flash of the LED visual alarm (about every 10 s). When the alarm is activated, more power is needed. Insufficient battery power is indicated by a short audible tone emitted about every 10 s; the battery should be replaced at the end of any sampling period if the low battery warning is activated. The industrial hygienist should be notified if this occurs.
- 4.2. Functional use - ALWAYS OBTAIN A PRINTOUT OF ANY USABLE STORED DATA PRIOR TO INSTALLING THE BLUE KEY.

---

Installation of the blue key puts the Datalogger into "Sleep-mode," turns off the display, and reduces power consumption.

---

To start the Logger-mode and reset (clear) the memory, align the blue key, insert it into the Datalogger, turn the knurled ring until it is tight, and then remove the key. This starts the datalogging. When doing this, data stored previously in the memory will be lost.

During data collection, the display will show consecutively: (1) the immediate concentration (displayed for 5 s), (2) a "running" TWA (displayed for 2.5 s), (3) the peak concentration recorded during the time period sampled (displayed for 2.5 s). The Datalogger stops sampling after 12 h and the display shows OFF. To terminate the logging function at any time, attach the red key and depress the button once. The display will then show a continuous monitoring of the immediate concentration of the environment [as discussed in (1) above]. Do not depress the red key again before transferring the data or the data may be lost.

#### 5. Data Recovery

##### 5.1. Precautions

DO NOT INSTALL THE BLUE KEY PRIOR TO DATA TRANSFER, or the stored data will be lost.

DO NOT TRANSFER DATA IN POTENTIALLY HAZARDOUS ENVIRONMENTS where a spark might cause an explosion.

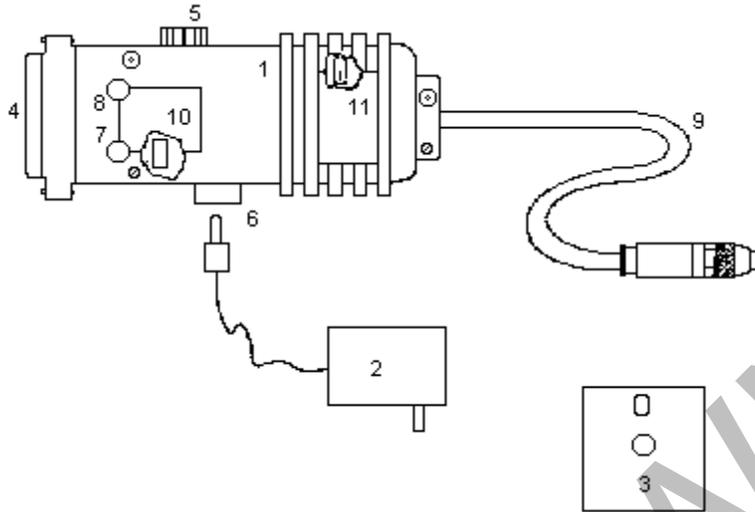


Figure 10

1. Converter Box.
2. 9V AC/DC Adaptor
3. Floppy disc, Enhanced Graphic Software
4. RS232 Interface Connector (female)
5. ON/OFF Switch (SW1) for starting transmission
6. AC/DC Supply Connector
7. "Power On" LED (green)
8. "Transmit" LED (red)
9. Interface cable to Model 190 Datalogger
10. Switch 2 (SW2) Selection Data Receive Line
11. Switch 3 (SW3) Connection DTR to ground

## 5.2. Computer equipment setup

- 5.2.1. Connect the RS232 connector of the Converter Box to the RS232 port of the computer (Figure 10). Use a suitable extension cable or adapter if needed.
- 5.2.2. Connect the AC/DC Adapter to the Converter Box and the power outlet, making sure the switch (SW1) on the side of the Converter Box is in the OFF position.

## 5.3. Programming of the computer

- 5.3.1. Load the MS-DOS system into the computer memory.
- 5.3.2. Load the Draeger EGS software into the computer (type EGS, press Enter).
- 5.3.3. When the Draeger logo appears on the screen, press any key. The following menu will appear:

### DATALOGGER ANALYZING SYSTEM COMMANDS

#### Commands:

- 0 = List files
- 1 = Quit
- 2 = Retrieve file
- 3 = Load from Logger
- 4 = Save file

5 = Display graph  
6 = Print Report  
7 = Configuration  
Type Command ->

#### 5.4. Data transfer

- 5.4.1. Connect the Converter Box cable to the Datalogger.
- 5.4.2. Press **3** (after Type Command ->) on the computer. This will set it up to receive data from the Datalogger.
- 5.4.3. Switch SW1 on the Converter Box to ON. The green LED will be lit. Data transmission will start automatically and the red LED will be lit. After a few moments, data transmission will be complete and the red LED will extinguish. At this point, switch SW1 to OFF. The data stored in the Datalogger will remain intact.
- 5.4.4. Default text information (from any previous data entry) will now appear on the screen. New text information can be added at this point:

Name	of user or operator
Location	where measured or headquarters
Date	when logged or downloaded
Start Time	when logging was started (military time format)
Comment	regarding this record
Gas	(select number from list)
Serial Number	of instrument used
- 5.4.5. Disconnect the Datalogger from the Converter Box. The data are now stored in the computer. The Datalogger should still have the data retained.
- 5.4.6. Screw the cap on the Datalogger key connection terminal. If data retention is no longer necessary and the monitor is to be stored, insert the blue key. This will reduce battery power consumption.

#### 5.5. Other DATALOGGER ANALYZING SYSTEM commands

---

Note: Check the configuration of the system before data transfer (press 7) to assure data will be deposited to the appropriate disk or area in the computer.

---

- 5.5.1. **Save file:** Press **4** and then enter a file name (up to eight characters). **Do not** supply the ".DAT" extension; this is added by the software. The data will be stored in the computer.
- 5.5.2. Commands used to retrieve data:
  - List files:** Press **0** to obtain a list of other Datalogger files in storage.
  - Retrieve file:** Press **2** to retrieve another set of data from storage and store it in the computer memory.
  - Display graph:** Press **5** to display the graph of CO concentration versus time. When the computer-printer system has been set up, follow the instructions to print a copy of the

graph. To obtain a vertical printout, press **F7**. To obtain a horizontal printout, press **F8**. To return to the menu, press **Enter**.

**Print report:** When a printer system is installed, press **6** to print a copy (spread sheet) of the complete list of the data from the Datalogger.

5.5.3. **Quit:** When data handling operations are complete, press **1** to exit from the EGS program.

WITHDRAWN

## Appendix C

### Calibration Gases from the OSHA Cincinnati Laboratory

The following gas blends containing CO are available for the OSHA offices. Orders may be placed through the regional offices, as for other supplies (5.24):

- BLEND #2 - Mixture of 35 ppm Carbon Monoxide, 1.6% Methane, 19.5% Oxygen and balance Nitrogen. The actual concentration of the Carbon Monoxide may vary between 35-40 ppm, the Methane between 1.5 -1.7%, and the Oxygen between 19.5% to 19.0%.
- BLEND #3 - 70 ppm ±5 ppm Carbon Monoxide in Air.
- BLEND #5 - Mixture of 50 ppm Carbon Monoxide, 0.55% ±.05% n-Hexane (50% of Lower Flammable Limit), 19.5% -.2% +0% Oxygen and the balance Nitrogen. [Note: Due to oxygen meter alarm characteristics, the oxygen range for this blend may not exceed 19.5% (+0%) and may not be lower than 19.3% (-0.2%).]

Examples of the labels which may appear on the BLEND #2 gas cylinders are shown below:

THIS CYLINDER CONTAINS THE NECESSARY CONCENTRATION OF THE LISTED GASES TO SPAN OR CHECK THE ALARM OPERATION OF THE FOLLOWING INSTRUMENTS:

DRAEGER MODEL 190 CO DOSIMETERMSA MICROGARD PORTABLE ALARMS  
SCOTT-ALERT MODEL S105ISC CMX270, 271 & MX241 MONITORS

THE INSTRUMENT MUST SEE THE CORRECT FLOW OR ERRORS IN READING THE GAS CONCENTRATIONS CAN OCCUR. USE THE APPROPRIATE REGULATOR THAT SUPPLIES EACH INSTRUMENT THE PROPER FLOW AS LISTED BELOW:

DRAEGER MODEL 190	200 sccm
MSA MICROGARD	200--250 sccm
SCOTT-LAERT MODEL S105	750--1000 sccm
ISC CMX & MX MONITORS	500-750 sccm

To re-order this cylinder thru the OSHA Cincinnati Laboratory, contact the ARA for Technical Support in your region. Order: BLEND #2. (Note: sccm = standard cubic centimeters per minute)

Approximate pressure	1000 psig
Approximate volume	100 liters @ 70°F

#### ANALYSIS

COMPRESSED GAS N.O.S.	UN1956
CARBON MONOXIDE	35.3 PPM
METHANE	1.59%
OXYGEN	19.5%
NITROGEN	BALANCE
Date shipped	10/16/91

Tables

Table 1a  
 Sampling and Analysis – TWA Output Values (Truncated)  
 [50% RH and 20-25 °C]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1 (0.5 × TWA PEL) ("A" experiment)	16.1	15	0.932					
#2 (0.5 × TWA PEL) ("A" experiment)	16.1	16	0.994					
#3(0.5 × TWA PEL) ("A" experiment)	16.1	16	0.994					
#4(0.5 × TWA PEL) ("A" experiment)	16.1	16	0.994					
#5(0.5 × TWA PEL) ("A" experiment)	16.1	17	1.056					
#6(0.5 × TWA PEL) ("A" experiment)	16.1	16	0.994					
				6	0.994	0.039	0.040	8.5
#1 (1 × TWA PEL) ("A" experiment)	39.2	36	0.918					
#2 (1 × TWA PEL) ("A" experiment)	39.2	37	0.944					
#3 (1 × TWA PEL) ("A" experiment)	39.2	37	0.944					
#4 (1 × TWA PEL) ("A" experiment)	39.2	38	0.969					
#5(1 × TWA PEL) ("A" experiment)	39.2	40	1.020					
#6(1 × TWA PEL) ("A" experiment)	39.2	38	0.969					
				6	0.961	0.035	0.036	11.2
#1 (2 × TWA PEL) ("B" experiment)	70.2	73	1.040					
#2 (2 × TWA PEL) ("B" experiment)	70.2	69	0.983					
#3 (2 × TWA PEL) ("B" experiment)	70.2	68	0.969					
#4 (2 × TWA PEL) ("B" experiment)	70.2	70	0.997					
#5 (2 × TWA PEL) ("B" experiment)	70.2	74	1.054					
#6 (2 × TWA PEL) ("B" experiment)	70.2	66	0.940					
				6	0.997	0.043	0.043	9.0

F/T = Found/Taken  
 OE = Overall Error (± %)  
 Bias = -0.016  
 CV<sub>2</sub> (Pooled) = 0.040  
 OE (Total) = ±9.6%

Table 1b  
 Sampling and Analysis - Hand-Calculated Average Values\*  
 [50% RH and 20-25 °C]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(0.5 × TWA PEL) ("A" experiment)	16.1	15.3	0.950					
#2(0.5 × TWA PEL) ("A" experiment)	16.1	17.0	1.056					
#3(0.5 × TWA PEL) ("A" experiment)	16.1	16.0	0.994					
#4(0.5 × TWA PEL) ("A" experiment)	16.1	16.0	0.994					
#5(0.5 × TWA PEL) ("A" experiment)	16.1	17.2	1.068					
#6(0.5 × TWA PEL) ("A" experiment)	16.1	16.1	1.000					
				6	1.010	0.044	0.044	9.8
#1(1 × TWA PEL) ("A" experiment)	39.2	36.0	0.918					
#2(1 × TWA PEL) ("A" experiment)	39.2	37.8	0.964					
#3(1 × TWA PEL) ("A" experiment)	39.2	37.0	0.944					
#4(1 × TWA PEL) ("A" experiment)	39.2	38.1	0.972					
#5(1 × TWA PEL) ("A" experiment)	39.2	40.1	1.023					
#6(1 × TWA PEL) ("A" experiment)	39.2	38.1	0.972					
				6	0.966	0.035	0.036	10.7
#1(2 × TWA PEL) ("B" experiment)	70.2	73.2	1.043					
#2(2 × TWA PEL) ("B" experiment)	70.2	69.5	0.990					
#3(2 × TWA PEL) ("B" experiment)	70.2	68.5	0.976					
#4(2 × TWA PEL) ("B" experiment)	70.2	70.6	1.006					
#5(2 × TWA PEL) ("B" experiment)	70.2	74.6	1.063					
#6(2 × TWA PEL) ("B" experiment)	70.2	66.7	0.950					
				6	1.005	0.042	0.042	8.8

F/T = Found/Taken  
 OE = Overall Error (± %)  
 Bias = -0.007  
 CV<sub>2</sub> (Pooled) = 0.041  
 OE (Total) = ±8.8%

\* Based on averages of all ppm values collected by each Datalogger

Table 2a  
 Sampling and Analysis - TWA Output Values (Truncated)  
 [50% RH and 20-25 °C, Low Concn]

Monitor	ppm Taken*	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(10 ppm) ("B" experiment)	11.1	10	0.901					
#2(10 ppm) ("B" experiment)	11.1	10	0.901					
#3(10 ppm) ("B" experiment)	11.1	11	0.991					
#4(10 ppm) ("B" experiment)	11.1	11	0.991					
#5(10 ppm) ("B" experiment)	11.1	11	0.991					
#6(10 ppm) ("B" experiment)	11.1	10	0.901					
				6	0.946	0.049	0.052	15.8
#1(5 ppm) ("B" experiment)	5.6	5	0.893					
#2(5 ppm) ("B" experiment)	5.6	5	0.893					
#3(5 ppm) ("B" experiment)	5.6	5	0.893					
#4(5 ppm) ("B" experiment)	5.6	5	0.893					
#5(5 ppm) ("B" experiment)	5.6	5	0.893					
#6(5 ppm) ("B" experiment)	5.6	4	0.714					
				6	0.863	0.073	0.084	30.6

F/T = Found/Taken

OE = Overall Error (± %)

\* Background CO is included in ppm Taken value. Background CO concentrations in the diluent air:

10 ppm experiment ~ 1.6 ppm CO

5 ppm experiment ~ 0.5 ppm CO

Table 2b  
 Sampling and Analysis - Hand-Calculated Average Values  
 [50% RH and 20-25 °C, Low Concn]

Monitor	ppm Taken *	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(10 ppm) ("B" experiment)	11.1	11.0	0.991					
#2(10 ppm) ("B" experiment)	11.1	10.8	0.973					
#3(10 ppm) ("B" experiment)	11.1	11.2	1.009					
#4(10 ppm) ("B" experiment)	11.1	11.4	1.027					
#5(10 ppm) ("B" experiment)	11.1	12.0	1.081					
#6(10 ppm) ("B" experiment)	11.1	10.6	0.955					
				6	1.006	0.045	0.044	9.5
#1(5 ppm) ("B" experiment)	5.6	5.0	0.893					
#2(5 ppm) ("B" experiment)	5.6	5.1	0.911					
#3(5 ppm) ("B" experiment)	5.6	5.2	0.929					
#4(5 ppm) ("B" experiment)	5.6	5.2	0.929					
#5(5 ppm) ("B" experiment)	5.6	6.0	1.071					
#6(5 ppm) ("B" experiment)	5.6	4.9	0.875					
				6	0.935	0.070	0.075	21.6

F/T = Found/Taken

OE = Overall Error (± %)

\* Background levels of CO in the generation stream are included in the Taken ppm value.

Table 3  
 Sampling and Analysis - Hand-Calculated Average Values  
 [50% RH and 20-25 °C, Ceiling Conc'n]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(Initial 5-min Period)	197.8	195.0	0.986					
#2(Initial 5-min Period)	197.8	191.4	0.968					
#3(Initial 5-min Period)	197.8	181.0	0.915					
#4(Initial 5-min Period)	197.8	198.6	1.004					
#5(Initial 5-min Period)	197.8	185.8	0.939					
#6(Initial 5-min Period)	197.8	189.0	0.956					
				6	0.961	0.032	0.033	10.5
#1(Start to End of CO Flow, approx. 50 min)	197.8	192.1	0.971					
#2(Start to End of CO Flow, approx. 50 min)	197.8	187.4	0.947					
#3(Start to End of CO Flow, approx. 50 min)	197.8	172.4	0.872					
#4(Start to End of CO Flow, approx. 50 min)	197.8	199.2	1.007					
#5(Start to End of CO Flow, approx. 50 min)	197.8	177.6	0.898					
#6(Start to End of CO Flow, approx. 50 min)	197.8	185.9	0.940					
				6	0.939	0.049	0.052	16.5
F/T	= Found/Taken							
OE	= Overall Error (±%)							

Table 4a  
Humidity Study - TWA Output Values (Truncated)  
[30% RH and 20-25 °C]

Monitor	ppm Take n	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(0.5 × PEL) ("B" experiment)	19.3	19	0.984					
#2(0.5 × PEL) ("B" experiment)	19.3	19	0.984					
#3(0.5 × PEL) ("B" experiment)	19.3	18	0.933					
#4(0.5 × PEL) ("B" experiment)	19.3	19	0.984					
#5(0.5 × PEL) ("B" experiment)	19.3	20	1.036					
#6(0.5 × PEL) ("B" experiment)	19.3	17	0.881					
				6	0.967	0.054	0.055	14.3
#1(1 × PEL) ("B" experiment)*	36.6	40	1.093					
#2(1 × PEL) ("B" experiment)*	36.6	40	1.093					
#3(1 × PEL) ("B" experiment)*	36.6	39	1.066					
#4(1 × PEL) ("B" experiment)*	36.6	40	1.093					
#5(1 × PEL) ("B" experiment)*	36.6	42	1.147					
#6(1 × PEL) ("B" experiment)*	36.6	40	1.093					
				6	1.097	0.027	0.024	14.6

F/T = Found/Taken

OE = Overall Error (± %)

Bias = 0.032

CV<sub>2</sub> (Pooled) = 0.042

OE (Total) = ±11.6%

\* Gas flow rate (1.310 L/min) over sensor was larger than calibration gas flow rate (0.60 L/min) (Ratio = 2.2). No compensation was made in the results for the different flows.

Table 4b  
Humidity Study - Hand-Calculated Average Values  
[30% RH and 20-25 °C]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(0.5 × PEL) ("B" experiment)	19.3	19.2	0.995					
#2(0.5 × PEL) ("B" experiment)	19.3	19.1	0.990					
#3(0.5 × PEL) ("B" experiment)	19.3	19.0	0.984					
#4(0.5 × PEL) ("B" experiment)	19.3	19.1	0.990					
#5(0.5 × PEL) ("B" experiment)	19.3	20.1	1.041					
#6(0.5 × PEL) ("B" experiment)	19.3	17.7	0.917					
				6	0.986	0.040	0.040	9.5
#1(1 × PEL) ("B" experiment)*	36.6	40.5	1.107					
#2(1 × PEL) ("B" experiment)*	36.6	40.8	1.115					
#3(1 × PEL) ("B" experiment)*	36.6	39.7	1.085					
#4(1 × PEL) ("B" experiment)*	36.6	40.6	1.109					
#5(1 × PEL) ("B" experiment)*	36.6	42.3	1.156					
#6(1 × PEL) ("B" experiment)*	36.6	40.5	1.107					
				6	1.113	0.023	0.021	15.5

F/T = Found/Taken

OE = Overall Error (± %)

Bias = 0.050

CV<sub>2</sub> (Pooled) = 0.032

OE (Total) = ±11.4%

\* Gas flow rate (1.310 L/min) over sensor was larger than calibration gas flow rate (0.60 L/min) (Ratio = 2.2). No compensation was made in the results for the different flows.

Table 5a  
Humidity Study - TWA Output Values (Truncated)  
[80% RH and 20-25 °C]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(0.5 × PEL) ("B" experiment)*	21.2	24	1.132					
#2(0.5 × PEL) ("B" experiment)*	21.2	22	1.038					
#3(0.5 × PEL) ("B" experiment)*	21.2	24	1.132					
#4(0.5 × PEL) ("B" experiment)*	21.2	25	1.179					
#5(0.5 × PEL) ("B" experiment)*	21.2	25	1.179					
#6(0.5 × PEL) ("B" experiment)*	21.2	23	1.085					
				6	1.124	0.055	0.049	22.2
#1(1 × PEL) ("A" experiment)	39.9	43	1.078					
#2(1 × PEL) ("A" experiment)	39.9	40	1.003					
#3(1 × PEL) ("A" experiment)	39.9	41	1.028					
#4(1 × PEL) ("A" experiment)	39.9	41	1.028					
#5(1 × PEL) ("A" experiment)	39.9	42	1.053					
#6(1 × PEL) ("A" experiment)	39.9	44	1.103					
				6	1.048	0.037	0.035	11.9
#1(2 × PEL) ("A" experiment)	74.4	82	1.102					
#2(2 × PEL) ("A" experiment)	74.4	74	0.995					
#3(2 × PEL) ("A" experiment)	74.4	74	0.995					
#4(2 × PEL) ("A" experiment)	74.4	78	1.048					
#5(2 × PEL) ("A" experiment)	74.4	75	1.008					
#6(2 × PEL) ("A" experiment)	74.4	69	0.927					
				6	1.013	0.059	0.058	12.8

F/T = Found/Taken

OE = Overall Error (± %)

Bias = 0.062

CV<sub>2</sub> (Pooled) = 0.048

OE (Total) = ±15.8%

\* Gas flow rate (1.340 L/min) over sensor was larger than calibration gas flow rate (0.580 L/min) (Ratio = 2.3). No compensation was made in the calculations for this.

Table 5b  
Humidity Study - Hand-Calculated Average Values  
[80% RH and 20-25 °C]

Monitor	ppm Taken	ppm Found	F/T	N	Mean	Std Dev	CV	OE
#1(0.5 × PEL) ("B" experiment)*	21.2	24.0	1.132					
#2(0.5 × PEL) ("B" experiment)*	21.2	22.6	1.066					
#3(0.5 × PEL) ("B" experiment)*	21.2	24.4	1.151					
#4(0.5 × PEL) ("B" experiment)*	21.2	25.2	1.189					
#5(0.5 × PEL) ("B" experiment)*	21.2	25.4	1.198					
#6(0.5 × PEL) ("B" experiment)*	21.2	23.4	1.104					
				6	1.140	0.050	0.044	22.8
#1(1 × PEL) ("A" experiment)	39.9	43.2	1.083					
#2(1 × PEL) ("A" experiment)	39.9	40.8	1.023					
#3(1 × PEL) ("A" experiment)	39.9	42.0	1.053					
#4(1 × PEL) ("A" experiment)	39.9	41.5	1.040					
#5(1 × PEL) ("A" experiment)	39.9	43.0	4.078					
#6(1 × PEL) ("A" experiment)	39.9	44.6	1.118					
				6	1.066	0.034	0.032	13.0
#1(2 × PEL) ("A" experiment)	74.4	82.4	1.108					
#2(2 × PEL) ("A" experiment)	74.4	75.0	1.008					
#3(2 × PEL) ("A" experiment)	74.4	74.5	1.001					
#4(2 × PEL) ("A" experiment)	74.4	78.6	1.056					
#5(2 × PEL) ("A" experiment)	74.4	75.4	1.013					
#6(2 × PEL) ("A" experiment)	74.4	69.8	0.938					
				6	1.021	0.057	0.056	13.2

F/T = Found/Taken

OE = Overall Error (± %)

Bias = 0.075

CV<sub>2</sub> (Pooled) = 0.045

OE (Total) = ±16.6%

\* Gas flow rate (1.340 L/min) over sensor was larger than calibration gas flow rate (0.580 L/min) (Ratio = 2.3). No compensation was made in the calculations for this.

Table 6  
Humidity Study - TWA Output Values (Truncated)

Level F test	F(calc)	F(crit)
0.5 × PEL	17.20*	6.36
1 × PEL	26.41	6.36
2 × PEL	0.27	10.04
<u>Recoveries %</u>		
30% RH	50% RH	80% RH
96.7	99.4	112.4**
109.7**	96.1	104.8
***	99.7	101.3
<u>Average</u>		
103.2	98.4	106.2

\* Large values appear to be due to variability in mean recoveries. This variability appears related to the degree of matching the calibration gas flow to the generation system gas flow over the monitor sensors.

If (Flow rate generation)/(Flow rate calibration) >1, then CO concn results will be high.

\*\* Results were high as explained above.

\*\*\* Data were not collected for this experiment.

Table 8a

Qualitative and Quantitative Detection Limits (Truncated TWA Output Values)

ppm	Values	Values	Values	Values	Values	Values	Std Dev
Blank	0	0*	0	0*	0*	0	0.000
5.6	5	5	5	5	5	4	0.408
11.1	10	10	11	11	11	10	0.548
16.1	15	16	16	16	17	16	0.632

\* Datalogger reported zero although a number of values of -1 were reported for the 1-min readings.

IUPAC Method using the equation:  $C = k(sd)/m$

Where:

C = the smallest detectable concentration an analytical instrument can determine at a given confidence level.

k = 3 (Qualitative detection limit, 99.86% confidence). = 10 (Quantitative detection limit, 99.99% confidence).

sd = standard deviation of blank readings.

m = analytical sensitivity or slope as calculated by linear regression.

Note: For the Dataloggers, the numerical responses (TWA values) are nearly the same as the input values (ppm); therefore, the slope is nearly equal to unity.

Minimum detectable signal (Qualitative detection limit):  $C = 3(0.408)/1.0008 = 1.2 \text{ ppm}$

For  $k = 10$  (Quantitative detection limit):

$C = 4.1 \text{ ppm}$  as a reliable detectable signal

Table 8b

Qualitative and Quantitative Detection Limits (Hand-Calculated Average Values)

ppm	Values	Values	Values	Values	Values	Values	Std Dev
Blank	0.00	-0.26	0.00	-0.42	-0.12	0.00	0.174
5.6	5.0	5.1	5.2	5.2	6.0	4.9	0.393
11.1	11.0	10.8	11.2	11.4	12.0	10.6	0.497
16.1	15.3	17.0	16.0	16.0	17.2	16.1	0.709

Minimum detectable signal (Qualitative detection limit):  $C = 3(0.174)/0.984848 = 0.5 \text{ ppm}$

For  $k = 10$  (Quantitative detection limit):

$C = 1.8 \text{ ppm}$  as a reliable detectable signal

WITHDRAWN