# Investigation of the Trench Collapse at I-95 on February 4, 2018, in Miami, FL

U.S. Department of Labor Occupational Safety and Health Administration Directorate of Construction

June 2018



Report Prepared by Alan Lu, Ph.D., P.E. Office of Engineering Services Directorate of Construction

## The Project

The project was the I-95 Miami rehabilitation project in Miami, Florida. Archer Western Contractors, Ltd. (Archer Western) was the contractor of the project. The project included the removal and replacement of concrete pavement within the established project limits, such as replacement of all asphalt shoulder pavement with full depth concrete shoulder pavement. The project also included drainage modifications and new concrete barrier walls in the center median of the I-95, see Figures 1 and 2.

After Archer Western installed the buried drainage pipe involved in the incident, video evidence from the pipeline video inspection indicated that the pipe was either damaged during construction or mis-installed. Therefore, Archer Western decided to open a trench to repair/replace the pipe, see Figure 3, and had its employees to hand-dig the trench along the concrete barrier wall. The trench was approximately three and one-half feet deep, approximately 2 feet 10 inches wide and more than one hundred and thirty feet long. The concrete barrier wall involved in the incident was approximately 121 feet long, see Figure 4.

#### The Incident

On February 4, 2018, around 3:00 a.m., two employees of Archer Western were inside the trench working on the pipe. The entire concrete barrier wall, approximately 121 feet long, collapsed into the trench killing the two employees who were in the trench.

### **Analysis and Discussion**

The trench cross section, shown in Figure 3, is based on the observations and measurements obtained from our field visit on February 6, 2018. The concrete barrier wall sat directly on the utility trench, which was backfilled with flowable fill. Other than the subgrade soil underneath, the concrete barrier wall was not supported by or secured to any other structures, such as an inlet or pavement shoulder, see Figures 4 to 6.

The loads imposed on the subgrade soil from the concrete barrier wall was not limited to the immediate area of the wall, but also extended some distance away from the wall. This distance can be estimated as being equal to the depth of the excavation. Thus, a critical plane is formed sloping up from the bottom of the excavation toward the wall at an angle of 45 degrees, see Figure 3. Since the footing of the concrete barrier wall remained completely above the critical plane, according to the discussions in the preamble to OSHA's excavation standards (at 54 Federal Register 45924, October 31, 1989), the stability of the concrete barrier wall was endangered by the excavation operations. Therefore, per OSHA standard CFR 1926.651(i)(1) support systems should have been provided to ensure stability of the concrete barrier wall to protect employees working the trench.

During our site visit, the excavated soil was classified as OSHA Type C soil according to the site conditions and natural characteristics of the earth deposits, see Figures 5 and 6. Based on the OSHA laboratory test (see Appendix A), the sample of earth deposits collected at the incident site was further classified as granular sand with no cohesion, corresponding to OSHA Type C soil.

The soil sample contained 91.7% sand and gravel. At the incident site, it was also observed that large clumps of excavated spoil broke into small pieces without difficulty. Besides, approximately 0.1 inches of rain fell within 24 hours of the incident (see Appendix B for national climatic data). These facts confirmed that the subgrade soil at the incident site was not able to sustain the concrete barrier wall when the collapse occurred.

#### **Conclusions**

Based upon the above, we conclude that:

- 1) The cause of the failure was the instability of the concrete barrier wall. The instability of the concrete barrier wall was caused by the trench excavation operations.
- 2) No support systems such as shoring, bracing, or underpinning were provided by Archer Western to ensure the safety of employees and the stability of the concrete barrier wall, prior to, during and after the trench was opened.
- 3) Archer Western violated the OSHA standard CFR 1926.651(i)(1) by not providing a support system, such as shoring, bracing, or underpinning to ensure stability of the concrete barrier wall for the protection of the employees.
- 4) Archer Western violated the OSHA standard CFR 1926.651(k)(1) by not conducting any inspection of the excavation and the adjacent areas by a competent person prior to the start of the work or as needed throughout the shift, on or prior to 02/04/2018.



Figure 1 Project site (courtesy of Google.com)

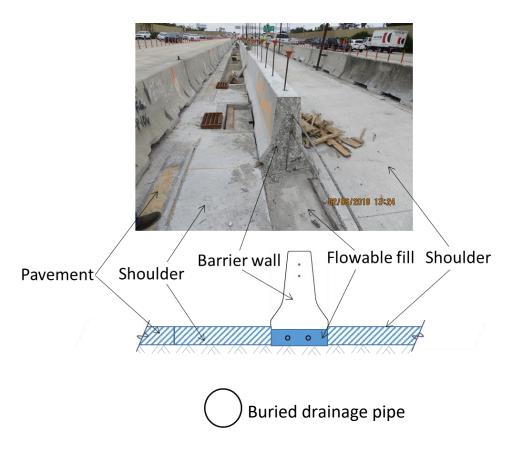


Figure 2 Typical section before excavation – looking north

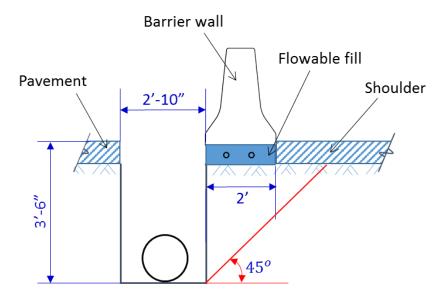


Figure 3 Typical section of the excavation prior to the collapse – looking north

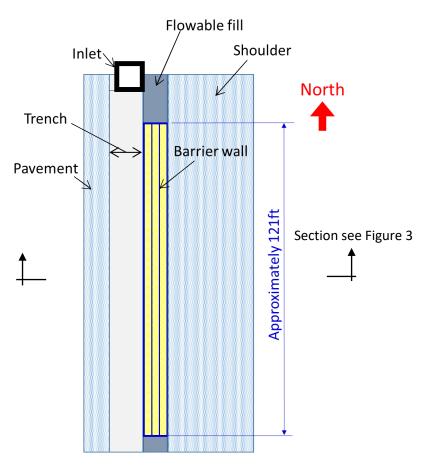


Figure 4 Plan view of the incident site



Figure 5 Scene of incident – looking south (North end of the barrier wall)



Figure 6 South end of the concrete barrier wall

#### Appendix A – OSHA Soil Laboratory Test Report

Air Sampling Report U.S. Department of Labor Occupational Safety and Health Administration. Page 1 of 3 2. Inspection Number 3. Sampling 1. Reporting ID 301406 418800 1293032 Number 4. Establishment Name Archer Western Construction, LLC 6. Sampling Date 5. CSHO ID 7. Shipping Date 8.Date Result Received J9763 06 FEB 2018 07 FEB 2018 11. Number Exposed 9. Job Title 10.Occupational Code Not applicable 12. Frequency of Exposure Exposure Summary Citation information 23. 16. 22. 17. Exp 18.Exp 19. 15. 14. Severity Rqstd Smpl Level Units PEL Adj No FTA Over PPE Trng Med OTH Type Eng Substance Code Type Cit Exp TWA calculated on actual time sampled The I. H. is free to make changes on the Form 91B and submit them directly to IMIS 26.Analyst's Comments OSHA ID-194 27. Chain of Custody Init. Date (Analytical Method) a. Seals Intact 20 MAR 2018 KAS b. Rec'd In Lab 26 MAR 2018 DJH c. Rec'd by Anal. Classification of S15809: 28 MAR 2018 DJH d. Anal. Completed Textural Structural: Granular SEA 28 MAR 2018 e. Calc. Checked ed as Type C 28 MAR 2018 f. Supr. OK'd because it contained 91.7% sand & gravel. 28 Submission HS-32 number 29 Lab Sample No. \$15809 (Minutes/Type) 30. Analyte 31. Analysis Results/ 32. Sample included in calculations of 9777 Soil N Because the results for air samples are used in further calculations, the number of figures reported in section 31 may not reflect the actual precision of the analysis. Calculated confidence limits (UCL & LCL) should be rounded to no more than three significant figures. The precision of analysis for wipe samples and for bulk material samples justify rounding results to no more than two significant figures.

The Sampling and Analytical Error (SAE) is the current value for the specific chemical(s) and should be used for the calculations.

Blank values are reported for reference only. Appropriate blank corrections have been applied to the samples by the Salt Lake Technical Center. Blank results are less than the reporting limit(s) unless otherwise noted.

33. Analyte Code SAE Value

S777

D L MILLIGRAMS PER LITER (URINE) MICROGRAMS PER DECILITER (BLOOD) PICO CURIES PER LITER (RADON GAS) PARTS PER MILLION FIBERS PER CUBIC CENTIMETER X MICROGRAMS M MILLIGRAMS PER CUBIC METER PERCENT Y MILLIGRAMS Ε FIBERS PER MM2 MILLION PARTICLES PER CUBIC FOOT (MPPCF) NONE

Sampling Number: 301406

## Appendix A – OSHA Soil Laboratory Test Report

Air Sampling Report U.S. Department of Labor Occupational

Occupational Safety and Health Administration.

Page 2 of 3

BM/S Bar Meters per Second

mcg/m Micrograms per Cubic Meter

Bulk samples are analyzed to provide an estimate of the composition of the material submitted. The results reported should be considered semi-quantitative only. Reporting limit for quartz in bulk samples is 1%

Analyte codes are chosen by the laboratory. The I. H. should review them for applicability. if there are any questions call the laboratory for appropriate analyte codes (ie. ICP uses fume analyte codes when the IH may have sampled for dust).

We value your comments regarding the customer support provided by the Salt Lake Technical Center Industrial Hygiene Chemistry Laboratory. You may leave comments (either positive or negative) with us at feedback.SLTC.IHC@dol.gov.

For questions regarding a specific case, please contact the Chromatography Group Manager, or the Spectroscopy and Physical Measurements Group Manager listed at http://intranet.osha.gov/dts/LAP/sltc.html.

Sampling Number: 301406

## Appendix A – OSHA Soil Laboratory Test Report

## **Permissible Exposure Limit Summary**

Office ID **Inspection Number** Sampled Establishment 418800

1293032 Archer Western 301406

Sampling Number

Construction, LLC

**Analyte Code Exposure Type** Unit PEL **PEL Severity** Req Sample Type Exposure

The following potentially applicable occupational exposure limits (OELs) are provided for reference only. OELs are not to be cited as OSHA standards. OELs referenced below can be a useful part of identifying the existence of a hazardous condition, but may not be sufficient alone to provide evidence of either hazard recognition or potential means of abatement.

**Analyte Code** Req Sample Type **Exposure Type Exposure** Unit REL **REL Severity Analyte Code** Req Sample Type **Exposure Type Exposure** Unit **TLV TLV Severity** 

## Appendix B - Local Climatological Data

National Centers for Environmental Information 151 Patton Avenue Asheville, North Carolina 28801

Local Climatological Data Daily Summary February 2018

U.S. Department of Commerce
National Oceanic & Atmospheric Administration
National Environmental Satellite, Data, and Information Service
Current Location: Elev. 29 ft. Lat. 25.7881° N Lon: -80.3169° W
Station: MIAMI INTERNATIONAL AIRPORT, FL US 12839

Minior   M																1			-		- Person	1014
Mail	o e		Temper	ature (F)			ē.6	gree Day ase 65F)		(LST)		Weather	<u> </u>	recipitati	on (in)	P. E.	ssure Hg)	Wind	D	rection =	Degree	
1								ပ				Weather Type	1				Avg		Peak Speed	Peak Dir	Sust. Speed	Sust. Dir
1		3								12		13	14				92		20	21	22	23
1		58*		0.0			0	3	0705				0.0	01		30.14		6.0	20	110	16	110
1		64		0.			9	8	0705	_	200		0.0	0,		30.12		3.6	15	300	10	110
1		19	7.1	6			9	9 (1	0704				1.0	2		30.14		80	25	100	2.1	100
1		69		00			0		0704				0.0	01		30.04		8.0	29	160	18	150
1		7.0		1.			0			_			0.0	0		30.06		6.2	21	080	17	080
1		70		9			0		0703	$\vdash$			-	-		30.19		10.5	19	060	16	060
1		72		3.5			0	1000					H	01		30.17		10.4	28	120	21	120
1		73		3.4			0				52-57		0.0	0,		30.17		9.1	18	060	15	080
National Control Con		72		53			0				-		0.0	4		30.16		11.8	25	070	20	100
1		72	H	1.2			0	22		-			-			30.12		12.8	29	120	21	110
1   1   1   1   1   1   1   1   1   1		75		0.1			ľ	_		$\vdash$	200		0.0	01		30.11		13.2	30	120	23	120
1		75		0.0			0	1883			.38		0.0	01		30.21		11.6	27	140	20	140
1	-	73		6.5			0				_33		0.0	0.		30.29		11.1	22	120	17	120
1		7.2		80			9	200					0.0	0.		30.29		10.2	22	110	18	120
1		19		7.5			9		1990	-			0.0	01		30.24		5.9	20	100	14	100
1	83	64		9.6			9		0656				0.0	0,		30.16		4.4	20	160	13	150
1	84	99		.5			9	22		-			0.0	01		30.16		5.2	25	170	15	130
1	84	70		5.4			9	8			-		0.0	0		30.17		9.0	28	060	18	120
1	84	7.0		5.4			0			-			0.1	0.		30.19		15.3	29	100	25	060
1	84	73	_	6.			9			-			Η.			30.24		17.3	30	120	23	100
1	83	74	-	7.2			9			$\rightarrow$	221		0.0	0		30.29		16.8	37	060	25	080
1	83	72	-	1.7			J						0.0	1		30.29		14.1	28	100	24	100
1	82	72		0.0			9	_					0.0	12		30.26		15.3	27	060	22	080
1	82	7.1		6			9	11	0649	-			T	17		30.15		13.2	27	100	22	110
1	82	7.1		6			9	2		-			T	20		30.13		6.6	26	110	16	100
5   1	84	7.1	Н	8.5			J	323					0.0	12		30.12		7.1	22	110	15	250
7.0   7.6   4.6   4.5	85*	89		2.3			9	2		-			0.0	91		30.12		6.3	24	080	17	060
700 763   701    702   703   702	81	+	-	91			3	1	0646	_			0.0	0		30.06		8.6	20	100	15	100
777   51   Degrete Days   Departure from Normal (1981-2010)   1-188   Number of days with   Neath of the complete of the comp	82.6	-	76.3	-	-	+	-	-	4		Monthly Ave	erages   Totals	0.3	73		30.17	30.21	10.1				
Monthly   Degree Days   Degr	4.5	7.7	6.1	X 100	82			0	epartur	e from	Normal (1981-2010)		-1.5	88	95.00							
Monthly Experimental Monthly Included Include			;	Degree	Days					-			Number	of days	with							
10tal Departure				thly	A POST OF CO.		Seas	on-to-da	e e					Prec	ipitation	_		Snow		We	ather	
317   146   465   0   0   0   7   2   0   0   1-Storins     317   146   465   0   0   0   7   2   0   0     317   146   465   0   0   0   7   2   0   0     317   317   318			Total	Depai	rture		otal	De	partnre	Ĭ	Max	oc c		1700			+		F			i
2009-07-14 Minimum 30.39 13 1165 Precip Station Augmentation Sea Lovel Pressure Sea Lovel Pressure Greatest Snowfall Greatest Sno	ealing		247	7-	0 4		101						553-	7-0.01	`	- 0		-	?	SILLIO	Пеал	/ rog
Maximum         30.39         13         Time         Precip         24-Hr           Minimum         30.00         04         1563         0.12         Date           Station Augmentation	Date of	5-sect	3-sec wil	nd equip	ment c	hande	3						•	2		1		Greate	est			
Maximum         30.39         13         1105         Precip         Snowfall           Minimum         30.00         04         1563         0.12         Date           Date           Station Augmentation												Date	Time				24-Hr			_		
30.00 04 1553 0.12 0.12 Station Augmentation			2009-07	7-14				Ma	ximum	H	30.39	13	1105		Pre	cip	H	Snow	rfall	<i>n</i>	пом пер	Ę
03-03								Z	nimum		30.00	90	1553		, O	12						
															03-	03		Dai	<b>.</b>			
											Station	2 Augmentation			1					- 6		

## Appendix B - Local Climatological Data

Minimate   Minimate	Location MIAMI P	Elev: 1(	urent Location: Elev: 10 ft. Lat: 25.6475° N Lon: -80.4331° W ation: MIAMI KENDALL TAMIAMI EXEC AIRPORT, FL US 12888	5.6475°	N Lon:	-80.433 )RT, FL	1° w US 128	88			Generated on 05/30/2018	35/30/2018									
Main   App   App		F	emperatu	ure (F)			Degre (base	e Days e 65F)		(LST)	5	Veather	Preci	pitation	(in)	Pressu (inHg			aximum M Directi	Vind Spee	d=MP
1	-	-		_				_	_	-	Wes	ather Type			Snow	-			ak sed Pe	sk Sust	οğ.
1	2			9	7	∞	6	10	Ξ	12		13			16	+			-	1	+-
1							0	2	0705	1806			00.0			30.16	10				10
1	82						0	9	0705	1806			00:00			30.14	4	_			30
1	74						0	<del>-</del>	0705	1807			0.02			30,15	0				60
1   1   1   1   1   1   1   1   1   1	80	200					0	0	0704	1808			00:0			30.08	00	-			14
1	85						0	10	0703	1808			00.00			30.08	9				180
1	78						0	9	0703	1809			00.00			30.21	0				60
1	82						0	10	0702	1810			њ			30.19	10				10
1	84						0	11	0702	1811			00:00			30.19	0		-		10
1	82	80					0	0	0701	1811			00:00			30.18	Σ				10
1   1   1   1   1   1   1   1   1   1	83						0	13	00.00	1812			0.01			30.14	1				12
1	84						0	13	0400	1813			00'0			30.12	12				14
1	84						0	13	0659	1813			00.00		arat.	30.22	10				12
1	84						0	11	0658	1814			0.01			30.31	1				10
1	83						0	o	0658	1815			Н			30.32	00	-			1
1	82						0	9	0657	1815			00:00			30.26	4				10
1	84		-				0	2	9990	1816			00:0			30.18	8	$\dashv$		_	13
1	83						0	7	0655	1816			00:00			30.18	4				12
1	83						0	7	0655	1817			00.0			30.19	7	-			60
1	82						0	1	0654	1818			60.0			30.21	13	-	+		10
1	82		1	_			0	13	0653	1818			0.12			30.26	14	+	+		-
1	84		+				0	13	0652	1819			00:0			30.30	15	-			60
7.0   7.6   6.9   7.0   1.1   0651   1820   NA   2.0   1.1   0651   1820   NA   2.0   1.1   0651   1820   NA   2.0   2.0   1.1   0651   1821   NA   2.0	84	+	+	_			0	13	0651	1820			0.11			30.31	14	+	+		19
1	83	1	-	_			0	-	0651	1820	$\neg$		0.12			30.27	13	+	+		60
1	82	1001					0	-	0650	1821			Н				12				11
1.5   1.5	84	77.00	-				0	7	0649	1821			Ts				00	+			11
1	838			2745			S)	88	0648	1822			0.54			30.14	3	-			28
1	85*						0	6	0647	1822	- 1		0.16			30.14	5	-		-	19
1	+	+	-				0	00	0646	1823			00:00			-	4	-	+	-	1
Monthly   Degree Days   Degr	+	~	2					•			Monthly Average	S Totals	1.185			-		=			
Monthly   Monthly   Season-to-date   Total   Departure   Maximum   Sea Level   Pressure   Time   Sea Level   Pressure   Time   Time   Sea Level   Sea Level   Time   Sea Level   Time   Sea Level   Time   Sea Level   Sea Level   Time   Tim		+		00000	6			ne	parrure	Hom	(0102-1381)		-1.32S	direct control	ا ا						
Total Moving         Procession of Section of			Month	an in	Days	0	0000	to date			F		io lacilin	uays wit							
1.55		Tota	5	Denart	d.I.	Lot	- le	Dens	artire				T	Precip	itation		Sno	>		Weather	
256         130         365         0         0         0         0         0         9         5         F         Present           5 Sec to 3-sec wind equipment change         Sea Level Pressure         Time         24Hr         Arthr         Annimum         30.38         14         1027         Precip         Snowfall         Snowf	ina			98-	2	146		1		,,	5	-	) I	01	)II \	1.1"	\ 1=4		T-Storn	-	avv Fo
Of 5-sec to 3-sec wind equipment change         Sea Level Pressure         Time         24.Hr           2009-02-13         Maximum         30.38         14         1027         Precip         Snowfall           Minimum         29.99         04         1617         0.54         Date	ling	258		130		365	10						0,	_		5					
Maximum         30.38         14         1027         Precip         Snowfall           Minimum         29.99         04         1617         0.54         Date	ate of 5-	sec to 3-	sec wind	equipr	nent ch	ange					Sea Level Pres	Ac	55					eatest		3	
Minimum         29.99         04         1617         Precip         Snowfall           26.26         Date         Date		g		9						-			me		1					Snow	Depth
25.59 U4 101/ U.54			2009-08-1	m				Max	mnm		30.38		027		Preci	۵	03	nowfall			
							1	Z Z		1	66.67		/10	1	0.04			Date			
																		2			

## Appendix B - Local Climatological Data

This math math math math math math math math	Main	National Environmental Saterlite, Data, and information Service Current Location: Elev: 10 ff. Lat.: 25.9069° N Lon: -80.2803° W Station: MIAMI OPA LOCKA AIRPORT, FL US 12882	ocation:	PA LO	CKA AI	Station: MIAMI OPA LOCKA AIRPORT, FL US 12882	FL US 12	2882					Generated on 05/30/2018	U <i>S/3U/2</i> U10									
Main	Main	Ою			Tempe	rature (F)	[02]		Degi (ba	ree Days se 65F)		(LST)		Weather	Precip	oitation (i		Pressu (inHg			mum Win Direction	d Speed =	MPH s
1	1												W	eather Type							Peak Dir	Sust.	Sust
1	1   1   1   1   1   1   1   1   1   1	-		3				8	6	10	£	12		13				-				. 22	23
No.   1	1			.99					0	2	0705	1805			00:00						100	16	130
1	1	02		09		3.0			0	9	0705	1805			00:00		60	0.15	4		300	14	290
1   1   1   1   1   1   1   1   1   1	1	03		65)		1.9			0	5	0704		SA BR		80:0		3	0.16	111		070	22	080
1	1	04		89		5.8			0	6	0704	1807			00:00		3	80.0	10		160	18	170
1	1	90		89		7.7			0	11	0703	1808			00:00		8	60.0	8		080	17	020
1	1	90		92		3.6			0	7	0703	1808			00:00		3	0.22	80		100	16	110
1	1	10		7.0		7.5			0	11	0702	1809			00:00		3	0.20	9.		130	21	110
1	1	80		19		7.4			0	17	0701	1810			00:00		8	0.21	7.		090	16	080
1	1	-	$\dashv$	70		7.3			0	Ξ	0701	-	4.A		ь		60	0.19	10		060	21	120
1	1	-	+	7.1		8.2			0	12	0700	1811			00:00		60	0.16	11		140	21	130
1	1	-	-	74	-	10.1			0	14	0700		3A		È		93	0.14	13		140	22	140
1	1					30.6			08	13s	0659	1812								20	120	15	120
1	1		H			6.8			0	13	0658	1813			00:00		8	0.33	10		100	17	120
1	1		+			8.9			0	Ξ	0657	1814								28	100	15	100
1	1	15	_	63	-	2.7			0	7	0657	1814			00:00		3	0.27	5.	-	110	14	110
1	1	16		09		2.6			0	7	9990	1815			00:00		60	0.19	4		190	14	150
1	1	17									0655	1816			00:00		60	0.19		21	150	16	110
1	1	18		19		6.4			0	-	0654	1816			00:0		63	0.20	7.		060	17	060
1	1	19		70		6.3			0	-	0654	1817	4.A		0.02		60	0.22	14		080	24	060
1	1	1	+	74	1	10.3			0	12	0653	1817			-		m	0.27	15		100	22	130
1	1	+	+	-	+	9.2			0	14	0652	$\neg$	2A		ь		6	0.32	15	+	110	24	060
1	1	22	1		+	8.1			0	13	0651	1819			F		60	0.32	13	-	080	22	080
1	1	23			1	7.0			0	12	0650	-	4A		E		60	0.28	13	-	110	22	060
1	1	24				7.9			0	13	0649	1820	SA		Ь		8	0.19	12		060	22	130
Since   12   12   12   13   14   15   15   15   15   15   15   15	Sign   1			89		5.8			0	1	0648	1820			Ě		8	0.15	∞		140	18	140
Signature   Sign	Signature   1822   RA			69		7.7			0	13	0648		4A		Ь		8	0.15	9		160	14	140
Sign   175	Sign   175   45   45   45   45   45   45   45			29		5.6			0	7	0647	1822	4.A		0.02		60	0.16	α .		080	20	080
17-4   7-1-4   1-4-4	1564   754   752	1	$\dashv$	+		4.5			0	10	0646	1822			F		60	$\rightarrow$	4		050	17	090
Sacrotuc and morning   1981-2010	Monthly   Degree Days   Degr		+	H	76.4					_			Monthly Averag	tes   Totals	0.048	_	8	-	4	9			
Monthly         Season-to-date         Temperature         Min         Frecipitation         Snow         Weath           10a         -30         115         >=90°         <=32°	Monthly   Departure   Total   Departure   Minimum   Society   Section 2.83   1.36   Section 2.84   Section 2.84   Section 2.84   Section 3.85   Section 3.85   Section 3.84   Section 3.85   Section 3.84   Secti				1.2	1				วั	parture	trom Nc	rmal (1981-2010)	:	-2.45s								
Monthly         Season-do-date         Tenperature         Minimum         Minimu	Monthly Age and Maximum         Season-do-date Departure         Imperature Departure         Maximum Monthly         Temperature Departure         Minimum Monthly         Temperature Departure         Maximum Minimum Monthly         Imperature Departure Departure         Minimum Monthly         Temperature Minimum Monthly         Monthly         Temperature Monthly         Temperature Monthly         Temperature Monthly				2	Degree	Days								lumber of d	ays with.	:						
10tal Departure   1154   115	10tal Departure   10tal Departure   115		1	ř	-60	nthly	4.100	F	Seaso	n-to-dat	0				_	Precipita	ation		Sno	2	×	eather	
130   130	280   -30   113   -280   -28			2	Ital	neball	e In	2	<u> </u>	neb	arrare	1	Max		, o		ļ		7		č	=	L
25ce to 3-sec wind equipment change         Sea Level Pressure         Time         24-Hr         Greatest           2009-07-08         Miximum         30.06s         28         1747         0.02         Date      Company   Compa	200         Of 5-sec to 3-sec wind equipment change         Sea Level Pressure         Time         2.4Hr         Greatest           2009-07-08         Minimum         30.38s         22         1041         Precip         Snowfall           Minimum         30.06s         28         1747         0.02         Date           Station Augmentation	Heat	5	Č	5 5	2 5	5 0	- 6	0 0			X.		25		5	i c		ï	će.	-Storms	Teav A	y rog
Maximum         30.06s         28         Time         Precip         24-Hr           Minimum         30.06s         28         1747         0.02         Date	Minimum         30.38s         22         1747         Precip         24-Hr           Station Augmentation         30.06s         28         1747         0.02         Date	و الم	ug te of 5-c	i of sec	2-coc w	C. C. Dai	ment ch	S SPECE	2				Sea Level Pre	Scenica	7		0		ē	reatect		-8	
Maximum         30.38s         22         1041         Precip         Snowfall           Minimum         30.06s         28         1747         0.02         Date	Minimum         30.38s         22         1041         Precip         Snowfall           Minimum         30.06s         28         1747         0.02         Date           Station Augmentation	S	5	200	4 200	1000	2	200	t				200	ate	ime			24.		odiosi			
Minimum 30.06s 28 1747 0.02 27-28	Minimum 30.06s 28 1747 0.02  Station Augmentation				2009-0	17-08				Max	imin		30.38s		041		Precin			lleJwou	T	Snow Dep	oth
27-28	Station Augmentation					}				Min	imum		30.06s		747		0.02						
														-						Date	100		
	Station Augmentation																27-28						